

то

TECHNICAL MEMORANDUM

DATE 26 May, 2023

Reference No. 22520011-TM

Ministry of Transportation and Infrastructure

CC Michael Carreira (Binnie), Robert McMahon (Ausenco)

FROM Emilio Martinez, MSc, PEng

EMAIL emilio.martinez@wsp.com

SILVER-SKAGIT ROAD FLOOD MITIGATION - 28.7 KM SITE HYDROTECHNICAL ASSESSMENT (REV 1)

1.0 INTRODUCTION

WSP has been retained by the Ministry of Transportation and Infrastructure (MOTI) to provide hydrotechnical engineering and design services for flood response mitigation and recovery works on the Silver-Skagit Road near Hope, BC. The project is divided into multiple sites depending on their location and level of urgency along the corridor. This memorandum describes the hydrotechnical considerations and assessment carried out to provide temporary mitigation design for the 28.7 km site.

The 28.7 km site requires temporary road surface repairs and culvert replacement, as well as restoration of the main drainage channel towards Klesilkwa Riveracross the Silver-Skagit Rd. The culvert replacement and road repairs are required due to washout from runoff and debris flows from the upper drainage across the Silver-Skagit Rd. The proposed temporary culvert replacement and channel restoration returns the main drainage path towards Klesilkwa River to its original path prior the November 2021 flood event. A permanent solution is planned for design and tendering in 2023. Road alignment, geotechnical design, fill materials and geometry for road repairs were provided by the Highway Design Engineer (R.F. Binnie & Associates Ltd.) and geotechnical consultant (Wood PLC), and are outside of the hydrotechnical scope of work.

2.0 SITE CLIMATE AND HYDROLOGY

2.1 General Climate and Precipitation

Based on the Köppen climate classification, Hope has an oceanic climate with warm summers and moderately cold winters. Temperatures in Hope over the course of the year typically range from -2 °C to 25 °C and are rarely below -10 °C or above 31 °C with a distinct warm season between June and September, and a cold season between November and February. The hottest month of the year is typically August with an average high temperature of 24 °C, and the coldest month is typically December with an average low of -2 °C.

The chance of wet days in Hope varies significantly throughout the year. The wetter season is typically between October and April with the wettest month generally being November with an average rainfall of 199 mm; the driest month is generally August with an average rainfall of 34 mm. Wet days are comprised of rain only, snow only, and rain and snow events. The month with the most snow is January, with an average snowfall of 276 mm.

2.2 Watershed Hydrology and Peak Flows

US-Canada border approximately 48 km south of Hope, BC; the river is approximately 26 km long from the upper reaches in the Cascade Range to Ross Lake and originates at around km 28 of Silver-Skagit Rd. The portion of the watershed draining to Klesilkwa River at the 28.7 km site is approximately 0.7 km² and consists of steep mountain terrain draining towards Klesilkwa River across the Silver-Skagit road. Similar to other tributary catchments, the area draining to Klesilkwa River at the 28.7 km site is subject to debris floods. The 28.7 km watershed exhibits elevations ranging from approximately 2045 masl, to 589 masl at the Silver-Skagit Road crossing.

WSP carried out an analysis of nearby hydrometric stations within 30 km of the site for unregulated streams to establish a relationship between the catchment area and peak flows based on historical flow measurements. The stations included in the analysis are Chilliwack River above Slesse Creek (08MH103), Coquihalla River above Alexander Creek (08MF068), Coquihalla River below Needle Creek (08MF062), Slesse Creek near Vedder crossing (08MH056), and Tulameen River below Vuich Creek (08NL071). For a contributing catchment of 0.7 km², the resulting 10-yr and 200-yr return period peak flows (Q10 and Q200) are approximately 0.8 and 1.8 m³/s, respectively, not accounting for climate change.

The location of the stations included in this analysis is shown in Figure 1. Although these gauges are for larger drainage areas, they have been selected to best represent potential runoff at this site and are considered to be adequate for the purposes of this report.

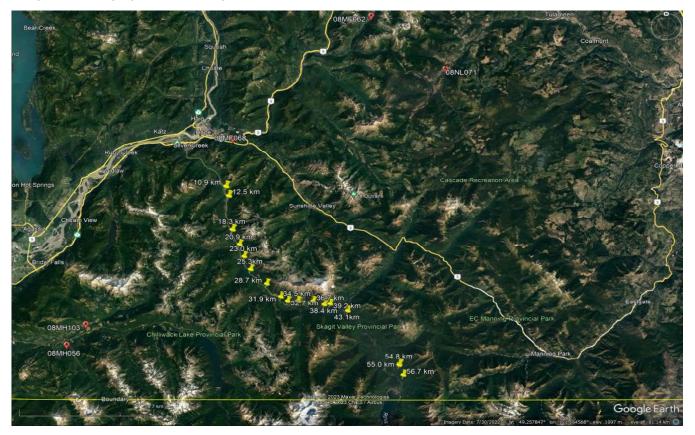


Figure 1 Hydrometric Stations near Hope, BC

2.3 Climate Change Considerations

Climate Change considerations within the design scope are applicable to small surface water drainage culvert sizing, water levels, erosion protection to the road embankment for the permanent design scope and estimates for the 200-yr return period peak flow. The temporary mitigation measures consider a Q10 without climate change considerations. This section provides a summary of the climate change assessment carried out for the conceptual mitigation design at the 28.7 km site, which follows the professional practice guidance from EGBC on climate change-resilient highway infrastructure (2020).

The Pacific Climate Impacts Consortium (PCIC) station hydrologic model outputs for historic (1981-2010), mid-century (2040-2069), and end-of-century (2070-2099) periods under RCP 4.5 and RCP 8.5 scenarios were used to estimate projected increases to streamflow for the 200-year return period event at four hydrometric stations: Fraser River at Hope, Coquihalla River above Alexander Creek, Harrison River near Harrison Hot Springs, and Chilliwack River at Vedder Crossing. It was assumed that the increase in streamflow for these larger rivers was applicable to the site catchment. The projected peak flows during a 200-yr return period event were estimated by applying the average median percent increase in streamflow for the RCP 8.5 end-of-century scenario between the four stations (18%) to the 200-yr flow rate under current conditions.

As a check to the projected flow increases based on the PCIC hydrologic model results, the IDF-CC Tool, Version 6.5, created by Western University was used to estimate projected precipitation increases for the area to the end of the century under RCP 8.5. The results indicate that 100-year, 24-hour events could increase in intensity by 19%, which is reasonably close to the results obtained with the PCIC data.

The resulting Q200 considering climate change is 2.1 m³/s.

3.0 HYDRAULIC ANALYSIS

WSP carried out a hydraulic analysis for the 28.7 km site to evaluate the design flow for the proposed culvert and channel replacement during the Q10 and Q200 events. The design peak flow was then used to size the proposed culverts, channel and provide erosion protection along the channel. The results of the analysis are summarized in the following sections.

3.1 Culvert and Channel Design

The resulting peak flow at the 28.7 km site during the Q200 was adjusted to account for potential debris floods at the culvert location. Based on a Melton ratio of 1.75 for the watershed, which corresponds to the potential for "debris floods", the water-only peak flow for the location was adjusted by a debris flood bulking factor of 2.0. Once adjusted, the Q200 flows for the culvert and channel at the 28.7 km site is 4.2 m³/s.

Several culvert type options were considered for the ultimate future replacement; the options included corrugated steel pipe (CSP) and pre-cast concrete box culverts. WSP carried out a hydraulic analysis for the proposed culvert configuration, with a resulting culvert sizing one pre-cast concrete box culvert barrel of 2200 mm (span) x 1800 mm (rise) for the Q200. No provisions for fish passage across the culvert have been accounted for, as no fish populations have been identified at the site. The culvert outlet velocity for the Q200 design flow has been estimated as 4.2 m/s.

In addition to the culvert design, WSP evaluated the required drainage channel size to convey the design flow into the proposed culvert. The resulting channel consists of a trapezoidal open channel with 2H:1V side slopes and a minimum base width of 3 m for the Q10 and Q200 design flows.

3.2 Avulsion Portection Berm

A diversion berm is proposed to direct main channel flows into the proposed culverts and to help prevent an avulsion that could result in flow directed to the road. The berm is approximately 55 m long and has a minimum 1.2 m height. The berm embankment consists of Type D fills with 2H:1V side slopes, and minimum and maximum crest widths of 1.0 m and 3.0 m, respectively. Riprap should be provided for erosion protection for the berm as described in Section 3.3.

3.3 Erosion Protection

Erosion protection to the drainage channel and diversion berm has been provided via a riprap layer. Riprap sizing has been estimated following recommendations from Section 1000 of the MoTI Bridge Design Specifications (MoTI, 2019, Section 1000) and the Transportation Association of Canada (TAC) design guidelines, for the Q200 design flow and channel configuration described above. The resulting riprap consists of Class 100 kg riprap and extends along the drainage channel up to 3.6 m upstream from the culvert inlet, 7.2 m downstream of the culvert outlet, and at the base of the diversion berm. Approximate rock particle mass and sizes for Class 100 kg riprap, based on spherical rock particles with a specific gravity of 2.50, are provided in Table 1.

Riprap sizing for the roadside ditch leading to the main channel was estimated from the catchment area contributing to the ditch (0.9 ha) and a longitudinal ditch slope of 4%; for a trapezoidal channel with a bottom width of 0.75 m and 2H:1V side slopes, the resulting riprap is Class 10 kg riprap. Rock particle sizes and gradation for the Class 10 kg riprap is provided in Table 2.

Percent Smaller (by Mass)	Mass (kg)	Intermediate Dimension (mm)
100	500	750
85	300	610
50	100	425
15	10	200

Table 1 – Class 100 kg Riprap Mass and Gradation

Table 2 – Class 10 kg Riprap Mass and Gradation

Percent Smaller (by Mass)	Mass (kg)	Intermediate Dimension (mm)
100	50	350
85	30	285
50	10	200
15	1	90

4.0 CLOSURE

We trust that this information is sufficient for your requirements. Should you have any questions regarding the above, or if you require further information, please do not hesitate to contact our office.

WSP CANADA INC.

te.p

Emilio Martinez, MSc, PEng *Hydrotechnical Engineer*

EM/KH



Kevin Henshaw, PEng Lead Hydrotechnical Engineer

WSP Canada Inc. (WSP) prepared this report solely for the use of the intended recipient, Ministry of Transportation and Infrastructure, in accordance with the professional services agreement. The intended recipient is solely responsible for the disclosure of any information contained in this report. The content and opinions contained in the present report are based on the observations and/or information available to WSP at the time of preparation. If a third party makes use of, relies on, or makes decisions in accordance with this report, said third party is solely responsible for such use, reliance or decisions. WSP does not accept responsibility for damages, if any, suffered by any third party as a result of decisions made or actions taken by said third party based on this report. This limitations statement is considered an integral part of this report.

The original of this digital file will be conserved by WSP for a period of not less than 10 years. As the digital file transmitted to the intended recipient is no longer under the control of Insert company, its integrity cannot be assured. As such, WSP does not guarantee any modifications made to this digital file subsequent to its transmission to the intended recipient.