# Geodetic Survey Division <br> Earth Sciences Sector 

# Cranbrook Calibration Baseline 1996 Adopted Values 

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## Baseline Site

The Cranbrook baseline is located on the north side of Highway \#95, about 10 km NE of Cranbrook.

This linear baseline consists of 5 concrete piers whose tops are about 1.5 meters above ground level. The piers are about 20 meters from the centerline of the highway and are accessible by vehicle. Some line clearing may be needed on a yearly basis.

See Appendix A for a plan and profile view of the baseline.

## Measurements

The 1996 measurements of this baseline were made by Hennessey from July 6-9, using the Mekometer ME5000 (serial number 357061). See Table 1 for the measurement history of this baseline.

Table 1: Measurement history

| Date | Observer | Instrument | Serial Number |
| :---: | :---: | :---: | :---: |
| July 23-26/1990 | Lafrance | Mekometer ME5000 | 357061 |
| Sept. 7-10/1991 | Lafrance | Mekometer ME5000 | 357061 |
| July 06-09/1996 | Hennessey | Mekometer ME5000 | 357061 |

Currently, each baseline measurement for a year consists of at least three double (forward and backward) distance measurements between all intervisible piers using either the Geomensor CR204 or Mekometer ME5000 EDM instruments.

## NGBL Calibration

The scale bias for the Mekometer ME5000 was determined from calibration surveys on the National Geodetic Baseline (NGBL). The constant bias from the NGBL was used as a gross check on the value determined from the Cranbrook baseline adjustment. The average scale bias from the two NGBL calibrations was applied to all distance observations. See Table 2 for the 1996 NGBL biases.

Table 2: Mekometer ME5000 biases derived from 1996 NGBL measurements

| Date | Measurement <br> Sets | Constant Bias <br> Value $\pm$ Std.Dev. (mm) | Scale Bias <br> Value $\pm$ Std.Dev. (ppm) |
| :---: | :---: | :---: | :---: |
| May 15-22 | 3 | $0.0 \pm 0.1$ | $-0.07 \pm 0.16$ |
| July 17-18 | 3 | $0.0 \pm 0.1$ | $-0.27 \pm 0.13$ |
| Average |  |  | $-0.17 \pm 0.15$ |

## Baseline Adjustment

The 1996 Cranbrook baseline measurements were processed with the new baseline adjustment program CALIB (version 1.1, May 95). A minimally constrained adjustment was made with pier 1 fixed. An a priori standard deviation of $0.1 \mathrm{~mm}+0.5 \mathrm{ppm}$ was used for all Mekometer distances, and 0.1 mm for the centering errors. The results of the 1990, 1991 and 1996 adjustments are summarized in Appendix B.

The constant bias from the CALIB adjustment was $-0.1 \pm 0.1 \mathrm{~mm}$, which is consistent with the estimate obtained from the NGBL calibration (see Table 2). The variance factor for the 1996 adjustment was 1.035 , which passes the Chi-square test. There were no residual outliers in the adjustment using all the observations. All residuals passed the Chisquare goodness-of-fit test for normal distribution. All tests were performed at the $95 \%$ confidence level.

## Comparison with Previous Epochs

The results of the 1990, 1991 and 1996 adjustments were compared to check for any scale differences and pier movements between epochs. The analysis was performed with the new baseline comparison program LINCOMP (version 1.3, May 95). For the adjustments and analyses of the measurements prior to 1996, the reader is referred to the reports issued for those years.

## Pier Movement Analysis

The pier movement analysis performed by program LINCOMP uses the "least absolute sum" (L1-norm) solution. Piers that are identified as having statistically significant coordinate differences are removed from the analysis by renaming them. The process is iterated until no outliers remain. The comparison of the 1990, 1991 and 1996 epochs shows no pier movement at this baseline.

## Scale Difference Analysis

Any scale difference between epochs is estimated with program LINCOMP using the least squares (L2-norm) solution with suspected pier movements removed. The estimated scale differences between the epochs are given in Table 3.

Table 3: Scale difference between epochs

| Comparison |  | Piers Used | Scale Change |  |
| :---: | :---: | :---: | :---: | :---: |
| From | To |  | $\begin{gathered} \text { Value } \pm \text { Std.Dev. } \\ (\mathrm{ppm}) \\ \hline \end{gathered}$ | 95\% Confidence Interval (ppm) |
| 1990 | 1991 | 1,2,3,4,5 | $-0.21 \pm 0.47$ | -1.12 to +0.70 |
| 1991 | 1996 | 1,2,3,4,5 | $-0.21 \pm 0.44$ | -1.07 to +0.65 |

## Adopted Distances

The Adopted Distances for the Cranbrook baseline are given in Appendix C and are based on the 1996 measurements. This appendix gives the adjusted interpier slope distances, estimated standard deviations and elevation differences.

## Recommendations

Since there is adequate redundancy provided by 5 stable piers to derive the constant and scale biases, a remeasurement is not necessary at this time and should be done only at the request of the controlling agency.

Hennessey/Bresee
February 1997



BASELINE NAME: CRANBROOK, B.C.

| Epoch <br> Dates | Degrees <br> of <br> Freedom | Variance <br> Factor | Statistical <br> Tests |  | Derived <br> Constant <br> $m m$ | Input <br> Scale | Comments |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | V.F. | G.O.F. | mm $\pm$ S.D. |  |  |  |  |

LEGEND: V.F. - Variance Factor Test
G.O.F. - Goodness of Fit Test

NOTE:
All statistical and outlier tests performed with a $95 \%$ Confidence Level.

BASELINE NAME: CRANBROOK, B.C.

Calib Version $1.1 \quad 1996$ Epoch
February, 1997
Geodetic Survey Division, Geomatics Canada

| From <br> Pier | To <br> Pier | Elevation Difference Metres (m) | Slope Distance <br> Metres (m) | Std Dev (mm) |
| :---: | :---: | :---: | :---: | :---: |
| 1 | $\begin{aligned} & 2 \\ & 3 \\ & 4 \\ & 5 \end{aligned}$ | $\begin{array}{r} -5.208 \\ -7.400 \\ -7.755 \\ 3.828 \end{array}$ | $\begin{array}{r} 89.4126 \\ 503.8104 \\ 707.1095 \\ 996.6949 \end{array}$ | $\begin{aligned} & 0.1 \\ & 0.2 \\ & 0.2 \\ & 0.3 \end{aligned}$ |
| 2 | $\begin{aligned} & 1 \\ & 3 \\ & 4 \\ & 5 \end{aligned}$ | $\begin{array}{r} 5.208 \\ -2.192 \\ -2.547 \\ 9.036 \end{array}$ | $\begin{array}{r} 89.4126 \\ 414.5009 \\ 617.8112 \\ 907.4713 \end{array}$ | $\begin{aligned} & 0.1 \\ & 0.1 \\ & 0.2 \\ & 0.2 \end{aligned}$ |
| 3 | $\begin{aligned} & 1 \\ & 2 \\ & 4 \\ & 5 \end{aligned}$ | $\begin{array}{r} 7.400 \\ 2.192 \\ -0.355 \\ 11.228 \end{array}$ | $\begin{aligned} & 503.8104 \\ & 414.5009 \\ & 203.3111 \\ & 493.0587 \end{aligned}$ | $\begin{aligned} & 0.2 \\ & 0.1 \\ & 0.1 \\ & 0.2 \end{aligned}$ |
| 4 | $\begin{aligned} & 1 \\ & 2 \\ & 3 \\ & 5 \end{aligned}$ | $\begin{array}{r} 7.755 \\ 2.547 \\ 0.355 \\ 11.583 \end{array}$ | $\begin{aligned} & 707.1095 \\ & 617.8112 \\ & 203.3111 \\ & 289.8513 \end{aligned}$ | $\begin{aligned} & 0.2 \\ & 0.2 \\ & 0.1 \\ & 0.1 \end{aligned}$ |
| 5 | $\begin{aligned} & 1 \\ & 2 \\ & 3 \\ & 4 \end{aligned}$ | $\begin{gathered} -3.828 \\ -9.036 \\ -11.228 \\ -11.583 \end{gathered}$ | $\begin{aligned} & 996.6949 \\ & 907.4713 \\ & 493.0587 \\ & 289.8513 \end{aligned}$ | $\begin{aligned} & 0.3 \\ & 0.2 \\ & 0.2 \\ & 0.1 \end{aligned}$ |

