File No.: 37457



July 12, 2023

McElhanney Ltd. Suite 500 – 3960 Quadra Street Victoria, BC V8X 4A3

Attention: Jack McKee, MESc., ENV SP., P.Eng

### FRASER VALLEY HIGHWAY 1 CORRIDOR IMPROVEMENTS ENVIRONMENTAL HABITAT ENHANCEMENTS – BRADNER NORTH & NATHAN CREEK

Dear Jack,

At the request of McElhanney Ltd. (McElhanney), Thurber Engineering Ltd. (Thurber) has completed a geotechnical assessment as part of the above-mentioned project in Abbotsford, BC. This letter outlines our understanding of the project, summarizes the results of our analysis, and provides geotechnical recommendations for detailed design.

It is a condition of this letter that the performance of Thurber's professional services is subject to the attached Statement of Limitations and Conditions.

# 1. PROJECT UNDERSTANDING

We understand that the British Columbia Ministry of Transportation and Infrastructure (BC MoTI) is planning to complete environmental habitat enhancements as part of the Fraser Valley Highway 1 Corridor Improvement Program. This includes two sites in the Township of Langley identified as Salmon Wetland #1 and #2, and two sites in Abbotsford identified as Bradner North and Nathan Creek. This report includes our assessment of Bradner North and Nathan Creek for McElhanney`s 100% detailed design submission to BC MoTI. The geotechnical assessment of the Salmon Wetland #1 and #2 sites is provided in a separate report.

The Bradner North enhancement area is located north of the existing and planned expansion of the Brader Rest Area. The enhancements include a new channel with side channels connecting the Bradner rest area to an existing channel to the northeast. One access road is proposed from the north side of the planned Bradner rest area expansion to where the new channel connects with the existing channel. A stop log weir structure is also proposed to be installed in the existing channel, approximately 5 m downstream from the connection with the new channel.

The Nathan Creek enhancement area is located northwest of the Highway 1 Bradner Road overpass and has existing access from Bradner Road. The proposed enhancements include a wetland which drains via a new channel following the natural downward grade to the west connecting with Nathan Creek. The combined new channel and Nathan Creek will continue



through the existing access road via a new culvert. A grade raise of the existing road is planned near the installation location of the new culvert. A stop log weir structure is also proposed downstream of the connection of the new channel and Nathan Creek.

Based on drawings for the 50% detailed design submission provided by McElhanney, the existing ground surface elevation at the Bradner North site varies between El. 93 m and El. 101 m, and the Nathan Creek site varies between El. 98 m, and 108 m. The proposed access road embankment slopes are drawn with slope ratios of 3 horizontal units to 1 vertical unit (3H:1V) and the proposed cut slopes for the side channels and the rock lined channel are 3H:1V and 2.5H:1V, respectively. The proposed culvert comprises typical 2800 mm x 1500 mm concrete box sections for a channel length of approximately 18 m including endwalls.

The stop-log weir structures consist of heavy duty composite reinforced lagging supported between a total of four 8x36 H-Piles embedded into the native surficial soil. The piles are shown with a stick-up of roughly 2 m above the bottom of the new channel with the lagging extending 0.9 m above the bottom of the channel. The downstream side of the weir includes 100 kg rip rap riffle with a 4H:1V slope parallel to the direction of the channel.

# 2. GEOTECHNICAL CONDITIONS

A site-specific geotechnical site investigation was not completed by Thurber for the environmental habitat enhancement areas. However, available geotechnical information as part of the Fraser Valley Highway 1 Corridor Improvement Program was considered sufficient for assessment of the geotechnical components of the detailed design. The degree of understanding for the enhancement areas discussed in Section 3.1 reflects the uncertainty of not completing a geotechnical investigation near the proposed infrastructure.

### 2.1 Surficial Geology

The Geological Survey of Canada (GSC) surficial geology map for Mission (Map 1485A) indicates both sites are underlain by the Fort Langley Formation (FLc). The specific formation at the sites includes glaciomarine stoney silt to loamy clay 8 m to 100 m thick.

### 2.2 Existing Geotechnical Information

Thurber completed geotechnical investigations for the functional and detailed design of the Fraser Valley Highway 1 Corridor Improvement Program. Geotechnical information was used from the following reports to infer the soil conditions at the habitat enhancement areas:

 "Fraser Valley Highway 1 Corridor Improvement Program - 264<sup>th</sup> Street to Watcom Road Segment 1, Geotechnical Investigation Factual Report" (2023) by Thurber



 "Highway 1 – 264 Street to Whatcom Road, WAR#4 – Bradner Road Rest Area Improvements, Geotechnical Report Issued for Tender" (2023) by Thurber.

The site investigation locations were generally within the Highway 1 right-of-way and the planned extents of the Bradner rest area expansion. The site investigations included test pits, cone penetration tests (CPTS), and solid stem auger, mud rotary and sonic test holes. The maximum depth of the investigation near the Bradner North site was 12 m below ground surface (Approximately EI. 89 m) and near the Nathan Creek site the maximum depth was 30 m (Approximately EI. 96 m).

The results of the geotechnical investigations considered relevant for the interpretation of the Bradner North and Nathan Creek enhancement areas are presented on the attached logs and CPT profiles. The logs provide detailed descriptions of the soil and groundwater conditions encountered near the Bradner rest area and Highway 1 Bradner Road overpass and should be used in preference to the generalized descriptions provided below. The following section provides a description of the inferred soil conditions at the sites for discussion related to the proposed enhancement area infrastructure.

### 2.3 Soil and Groundwater Conditions

### 2.3.1 Bradner North Enhancement Area

The soil conditions at the Bradner North site are inferred to comprise organic silt overlying silty clay to depths greater than 12 m. The depth to more dense, competent soil is unknown based on the available geotechnical information and is not expected to influence the design of the enhancement area.

The test holes and test pits completed for the Bradner rest area expansion indicate that the organic silt layer is soft and approximately 0.5 m to 0.9 m thick. Considering the proximity of these holes to the planned enhancement area, similar thicknesses of this layer can be assumed for the enhancement area. The water content of the organic silt ranges from 58% to 78%.

The underlying silty clay is considered stiff to very stiff with interpreted undrained shear strengths between 75 kPa to 100 kPa. The water content of this layer ranges from 21% to 27%. Atterberg limit testing indicates liquid limits between 31% to 33%, and plastic limits between 18% to 21%.

Groundwater level observations for the Bradner rest area expansion measure the water level between surface and a depth of 1.8 m. These measurements have been inferred to represent a perched groundwater table at the site that is expected to fluctuate seasonally. In general, the provided winter and summer average, and 2-year water surface elevations were used to guide



the geotechnical analysis for drained conditions and assumed groundwater table depth of 1 m was used for undrained conditions.

### 2.3.2 Nathan Creek Enhancement Area

The test holes for interpretation of the Nathan Creek site were generally located within the Highway 1 right-of-way where stripping is presumed to have been completed before placement of fill. Therefore, organic soils were not observed either at ground surface or underlying the fill materials at these locations. However, at the Nathan Creek site, it has been inferred that the soil conditions comprise organic soils overlying silty clay and thick, alternating layers of silt and sand.

The silty clay is assumed to be stiff near ground surface with consistency increasing with depth to very stiff. Similar to the Bradner North site, the undrained shear strengths have been assumed between 75 kPa to 100 kPa, even though interpretation from the CPTs and attempted vane shear tests (VST) closer to the Bradner Road Overpass indicate the undrained shear strengths likely exceed 100 kPa. Water contents ranged between 17% and 32% and Atterberg testing results indicate liquid limits between 27% and 36% and plastic limits between 17% and 26% for this layer.

Alternating layers of sand and silt were encountered at a depth of 16 m (Approximately EI. 96 m) at TH21-04 in the westbound right-of-way of Highway 1. The alternating layers were up to 3 m thick and continued to the maximum depth of the test hole. Varying amounts of gravel were observed in the sand layers. The beginning of a sand layer was also observed at the same elevation near the termination depth of TH22-SEG1-47. The sand is considered dense based on standard penetration test (SPT) results. Depending on the extent of these sand layers, it is possible that dense gravelly sand could be encountered a few meters below ground surface near the end of the new channel where the stop-log weir structure and box culvert are planned.

### 3. GEOTECHNICAL ANALYSIS

### 3.1 Design Criteria

Consistent with the BC MoTI Geotechnical Design Criteria (Technical Circular T-04-17), the geotechnical analysis was completed with consideration of the following design guides and codes:

- Canadian Highway Design Bridge Code (CSA-S6-19)
- BC MoTI Supplement to CSA-S6-19
- BC MoTI Pavement Structure Design Guidelines (Technical Circular T-01/15)
- Canadian Foundation Engineering Manual (4<sup>th</sup> Ed., 2006)

Given the distance to available geotechnical site investigation information, a "Low" degree of understanding was used for analysis and design. A "Typical" consequence factor was applied for



the design of the access roads. The use of a "Low" consequence factor was considered for the cut slopes where nearby infrastructure or roads are unlikely to be affected. We consider this appropriate for the project intent of re-establishing more natural terrain where minor sloughing of slopes are not likely to affect the function of the habitat enhancement area and can be repaired if needed. McElhanney should confirm with BC MoTI if the use of a "Low" consequence is considered acceptable for this circumstance.

As directed by McElhanney, seismic loading on the proposed access roads, cut slopes and culvert were not included in our geotechnical analysis.

# 3.2 Slope Stability

The slope stability of the proposed access road and channel cut slopes was assessed using the limit equilibrium analysis software Slide2 (Build 9.023) by Rocscience Inc. The estimated geotechnical soil parameters used in the analysis for drained and undrained conditions are summarized in Table 1. Where applicable, a surcharge load of 16 kPa was included to represent construction and maintenance equipment traffic.

Material Name	Unit Weight (kN/m³)	Friction Angle (degrees)	Undrained Shear Strength (kPa)
Granular Fill	20	38	-
Silty Clay	19	30	75
Rip Rap	22	45	-

 Table 1: Estimated soil parameters for slope stability analysis

The target factors of safety (FOS) for global stability given the degree of understanding and consequence factors are summarized in Table 2 (BC MoTI Supplement to CSA-S6-19 Table 6.2B). The permanent FOS was considered applicable for drained conditions and the temporary FOS was considered applicable for undrained conditions.

 Table 2: Factors of Safety for Global Stability (BC MoTI Supplement to CSA-S6-19)

	Degree of Ur	nderstanding
Factor of Safety for	Lo	DW
Global Stability	Conseque	nce Factor
	Typical	Low
Permanent	1.67	1.45
(Drained)	1.07	1.45
Temporary	1.43	1.24
(Undrained)	1.45	1.24



### 3.3 Settlement Analysis

Settlement analysis of the proposed access road and culvert was completed using the software Settle3 (Build 5.020) by Rocsience Inc. The estimated primary and secondary consolidation parameters used in the analysis are summarized in Table 3. These parameters were based on 1D consolidation test results from the Fraser Valley Highway 1 Corridor Improvement Program - 264<sup>th</sup> Street to Watcom Road Segment 1. The analysis was completed assuming steady state conditions (i.e. time-dependent parameters were not included) for estimating long-term settlement magnitudes.

Material Name	Unit Weight (kN/m³)	Comp. Index (Cc)	Recomp. Index (Cr)	Initial Void Ratio (e₀)	OCM¹ (kPa)	Secondary Consolidation Ratio (Cα/Cc)
Silty Clay	19	0.23	0.03	0.8	200	0.035

Table 3: Estimated geotechnical parameters for settlement analysis

Note: 1) Overconsolication Magnitude

The access roads and concrete box culvert were applied as surcharge loads at ground surface and the channel bottom elevation, respectively. The access road surcharge was estimated assuming a soil unit weight of 20 kN/m<sup>3</sup> and the maximum height of the fill provided on the 50% detailed design drawings. The concrete box culvert self-weight was estimated based on values for typical sections provided by local manufacturers.

# 3.4 Lateral Resistance of Piles

The lateral resistance of the proposed piles for the stop-log weir structures was completed using the software RSPile (Build 3.018) by RocScience Inc. The non-linear load (p) versus deflection (y) curves applied to the soil were based on an undrained shear strength of 75 kPa and associated default strain factors recommended in the RSPile manual by RocScience.

The estimated force per pile for the analysis was estimated based on the hydrostatic force applied over the height stop-log lagging and evenly distributed to the appropriate number of piles. Given a "Low" degree of understanding for the site, geotechnical resistance factors of 0.45 and 0.7 were used for analysis of the lateral resistance and lateral deflection, respectively.



# 4. GEOTECHNICAL DISCUSSION AND RECOMMENDATIONS

### 4.1 Cut Material Reuse as Fill

The in situ water content of the native silty clay is expected to be between 20% and 30%. These water contents are likely much higher than the optimum water content required for adequate compaction. Given the moisture sensitivity of this material and the challenges associated with drying and maintaining the material for reuse, we do not recommend the reuse of the excavated silty clay for access road embankment construction. However, if the contractor can dry the material within 2% of the optimum water content, it could potentially be used for berms less than 1.5 m high planned along the parts of the new channel.

### 4.2 Access Roads

### 4.2.1 Bradner North Enhancement Area

The subgrade of the access roads should be stripped of vegetation, topsoil and organic material to expose the stiff silty clay. The exposed subgrade is expected to be susceptible to disturbance from rain and construction traffic. Therefore, we recommend limiting construction traffic on the subgrade and considering placement of fill shortly after stripping activities.

All embankments should be constructed in accordance with BC MoTI standard specifications. The access road fill below the proposed pavement structure should comprise well-graded granular material such as 75 mm minus pit run sand and gravel. The fill should be placed in 200 mm maximum thick loose lifts and compacted to 95% standard Proctor maximum dry density (SPMDD).

We understand the typical section for a Type C or Type D Pavement Structure is considered appropriate for the expected maintenance traffic and site conditions. Given the expected silty clay (CL) subgrade at Bradner North, the select granular subbase (SGSB) layer should be a minimum of 300 mm thick. Where access road fill is not required to reach final grades with the proposed pavement structure, a non-woven geotextile should be placed as a separator between the SGSB layer and the silty clay subgrade. Based on the results of the slope stability analysis, access road embankment slope angles of 3H:1V or flatter are considered appropriate.

Immediate settlement of the access road is expected during construction but will likely not have significant effects on the final grade. Consolidation settlement of the compressible silty clay should be considered in the design and function of the access road. Consolidation settlement due to the self-weight of the road is estimated to be in the range of 25 mm to 50 mm, where fill heights are between 0.75 m and 1.5 m. Due to the variability in existing ground elevations along the access



road and the uncertainty regarding the site conditions, there is a potential for differential settlement along the access road alignment. A graded aggregate seal (GAS) or high fines gravel surface (HFSA) are considered suitable for accommodating the estimated settlement. Surface regrading may be required as future maintenance.

# 4.2.2 Nathan Creek Enhancement Area

The access road grade raise near the proposed culvert is expected to require surface preparation depending on the type of road surfacing and quality of the existing road embankment fill. In general, the road surface should be stripped of organic, loose and deleterious material before placement of access road fill or pavement structure materials. Further subexcavation may be required if unsuitable soils are encountered.

The access road fill and typical pavement structure recommendations for the Bradner North site are also considered applicable for the Nathan Creek site. If the access road comprises suitable coarse-grained material for subgrade, the SGSB pavement layer can be reduced to 150 mm thick. The consolidation settlement estimates for the Bradner North site are also considered applicable for the Nathan Creek site.

### 4.3 Cut Slopes

The cut slopes in the Bradner North and Nathan Creek habitat enhancement areas have been divided into two typical sections. The first typical section is the rock-lined channel which includes 2.5H:1V cut slopes up to 3 m high and lined with 450 mm of 25 kg rip rap. The minimum factor of safety for this typical section was 1.46.

The second typical section is the side channel with optional spawning gravel which includes 3H:1V cut slopes up to 5 m high and partially lined with 200 mm of round rock. The optional spawning gravel is proposed to be 500 mm thick and extend across the base of the channel only. The minimum factor of safety for this typical section was 1.47.

The slope stability analysis results meet the required factors of safety for permanent conditions with a "Low" degree of understanding and a "Low" consequence factor. Generally, further flattening the slopes improves the factor of safety. It should be noted that a minimum 2.5H:1V slope along the channel profile should also be maintained where the typical rock-lined channel section is being constructed.

### 4.4 Concrete Box Culvert and Endwalls

The subgrade for the concrete box culvert and endwall is expected to comprise the stiff silty clay. We recommend the placement of a granular working pad over the subgrade for construction of



the culvert and endwall. The recommended working pad specifications will depend on the amount of seepage entering the excavation.

If the excavation is relatively dry, the subgrade should be subexcavated and replaced with a minimum of 300 mm of well-graded sand and gravel. If the excavation is wet and the subgrade is easily disturbed, we recommend subexcavating and placing a minimum of 300 mm clear crush gravel fully wrapped with a non-woven geotextile. In both cases, the working pad should be compacted with light compaction equipment such as a 200 lb plate tamper only until the material "locks up". Over compaction could result in reduced density of the working pad and underlying subgrade. Deeper subexcavation typically develops more challenges in wet excavation conditions, and therefore subexcavation should not exceed 600 mm.

Provided that the subgrade and working pad are prepared as described above and the base of the culvert and endwalls are embedded a minimum of 0.5 m below the channel bottom, a factored bearing resistance 150 kPa is considered suitable for the ultimate limit state (ULS). A geotechnical resistance factor of 0.45 was used for "Low" degree of understanding. Assuming a target elastic settlement of approximately 15 mm, a bearing resistance of 100 kPa is considered suitable for the serviceability limit state (SLS).

Total consolidation settlement estimated at the base of the box culvert and endwalls is expected to be in the range of 25 mm to 50 mm. This settlement is expected to be relatively uniform along the culvert alignment due to the locations of the heavier loading from the endwalls and the load contribution from the access road in the middle of the alignment. If the magnitude of settlement exceeds the tolerances of the structural or functional aspects of the box culvert, preloading could potentially be used to mitigate the amount of settlement. However, preloading was not included in our assessment.

Backfill around the culvert and endwalls should comprise well-graded granular material (e.g. 75 mm minus pit run sand and gravel) placed in 200 mm thick lifts and compacted to 95% SPMDD.

# 4.5 Stop-Log Weir Structure

The HP 8x36 piles for the stop-log weir structure are considered suitable for resistance of hydrostatic loads. The piles should be installed with a minimum toe embedment of 4 m below the channel bottom to develop the required geotechnical resistance. Given this embedment, the lateral deflection of the pile head with a 2 m stick-up above the channel bottom is estimated to be less than 25 mm.



The piles can be installed using vibratory or impact driving methods. The proposed installation method and equipment should be reviewed with the contractor prior to mobilization. There is a possibility that the dense sand layer observed near the highway (TH22-SEG1-47) could also be present near the lower surface elevations of the Nathan Creek site where the stop-log weir is planned. Encountering this layer could result in early refusal of the piles during installation. The contractor should provide alternative options for installation to the minimum toe embedment if this occurs.

### 4.6 Construction Review

During construction, Thurber should be given the opportunity to review the exposed subgrade for the access roads, concrete box culvert and endwalls to confirm our design assumptions before placement of fill or geotextile. If required, Thurber can also provide review of imported material proctor, gradation and density test results completed by others.

### 5. CLOSURE

We trust this information meets your current needs. If you have any questions, please contact the undersigned at your convenience.

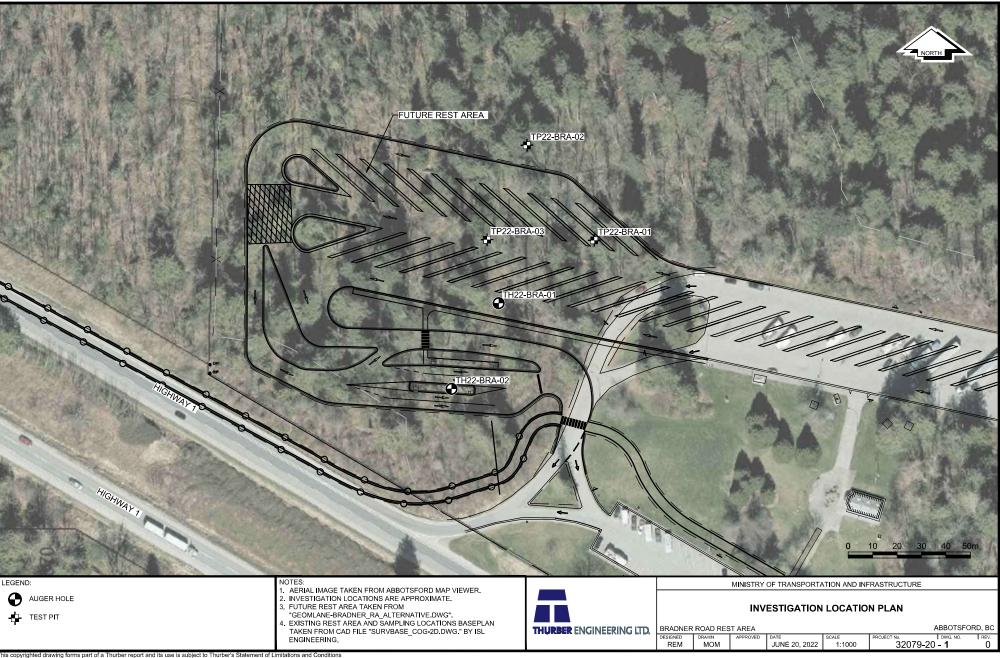
Yours truly, Thurber Engineering Ltd. Paul Evans, M.Eng., P.Eng. Review Principal

Thurber Engineering Ltd. Permit to Practice #1001319

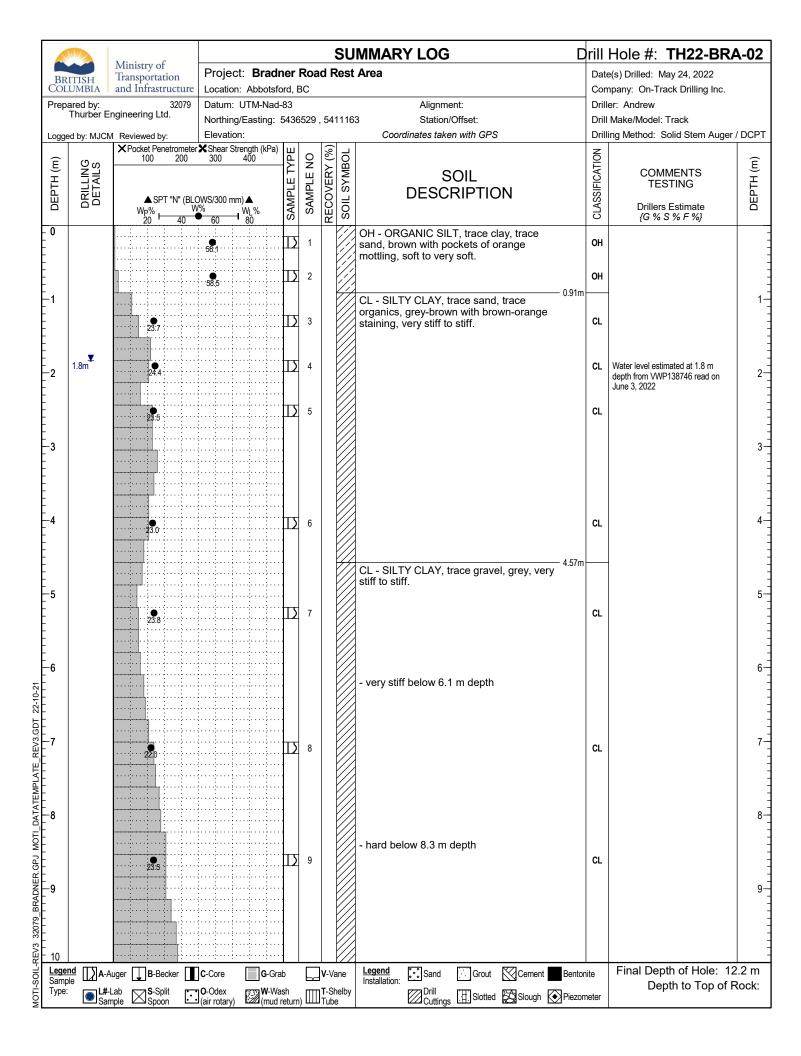
Kurt Baia, M.Eng., P.Eng. Geotechnical Engineer

Attachment

- Statement of Limitations and Conditions
- Highway 1 264<sup>th</sup> Street to Watcom Road Site Investigation Results
- Slope Stability Analysis Outputs



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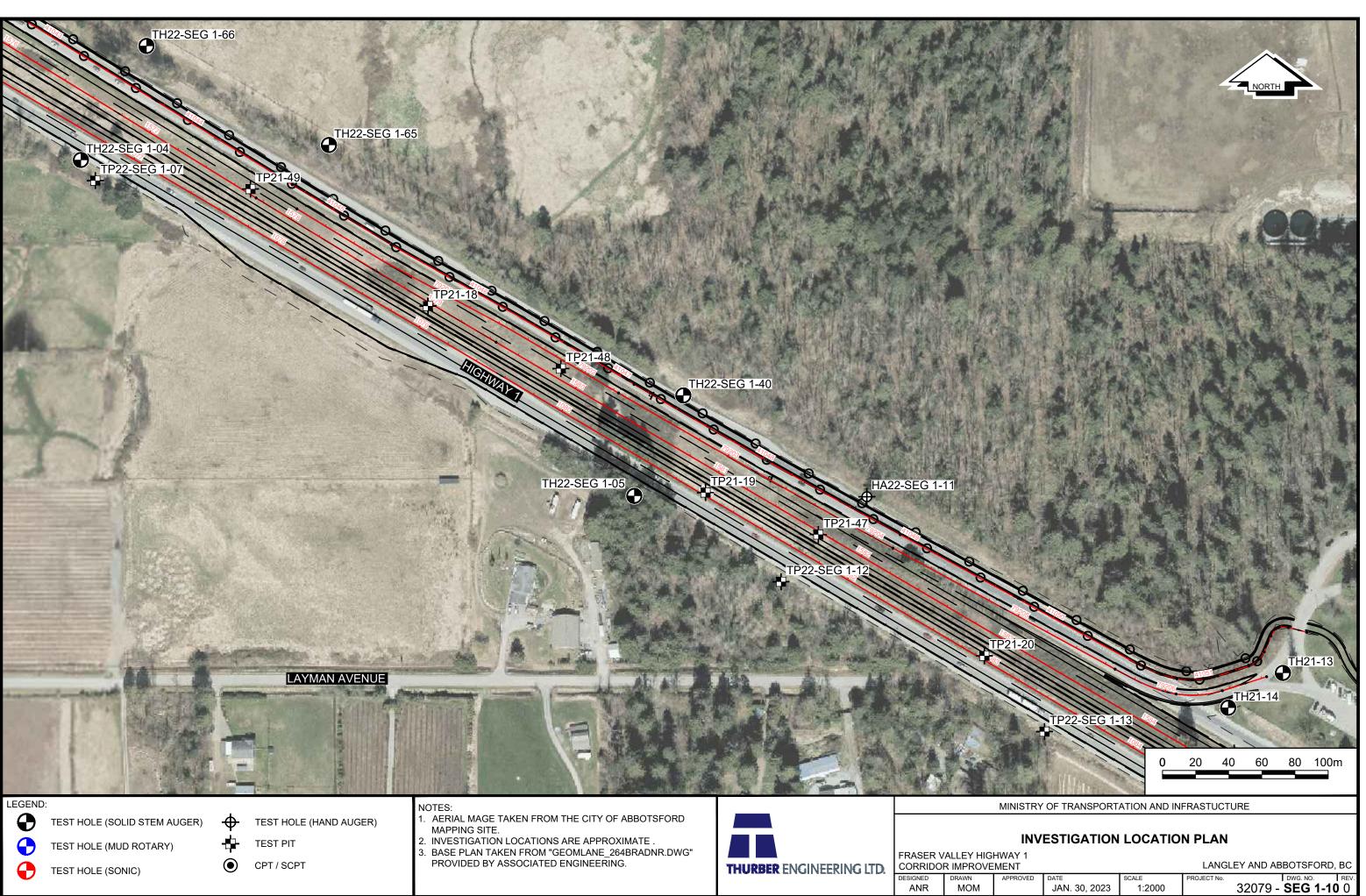


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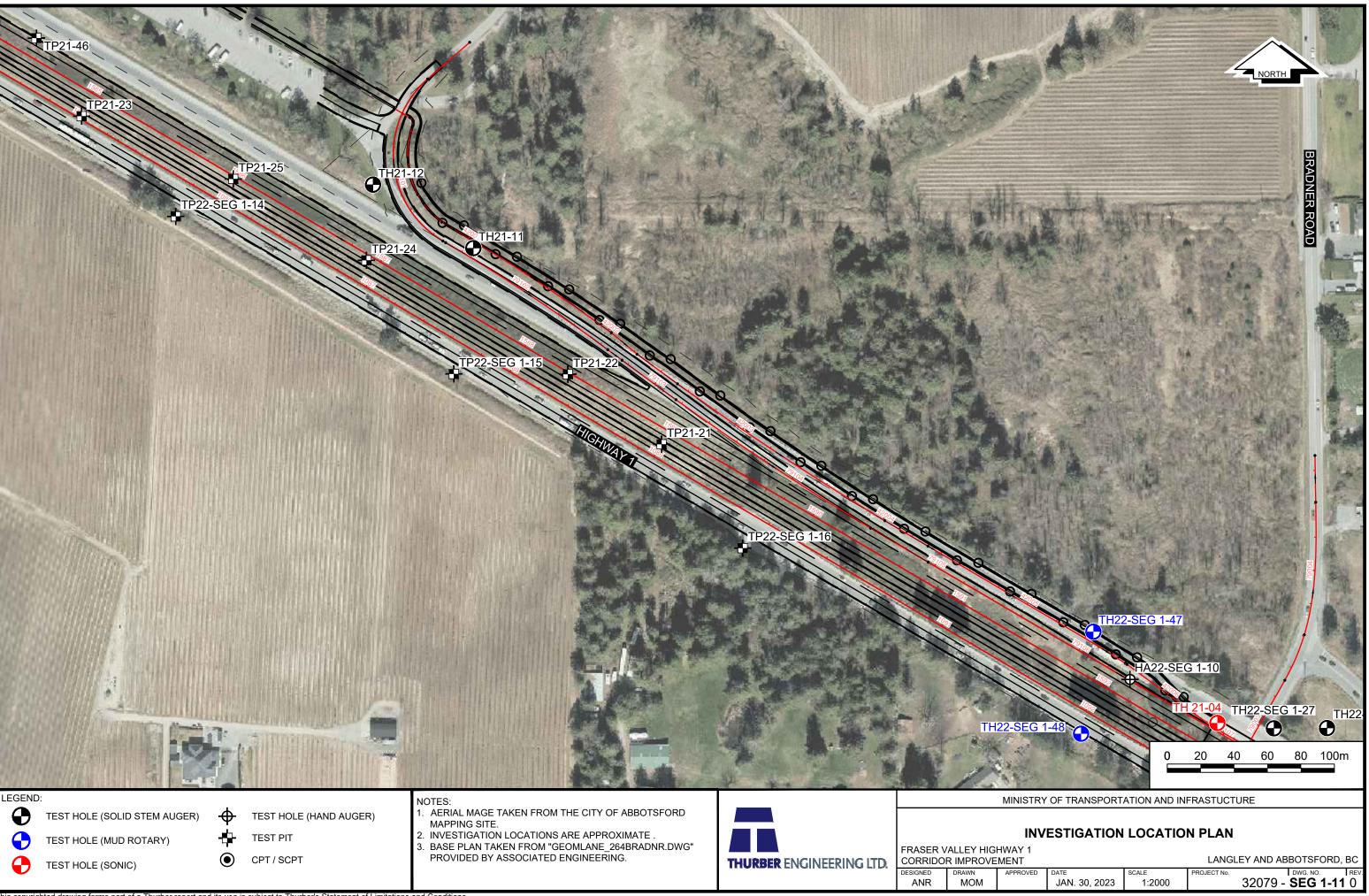
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10 Legen		Auger <b>B</b> -Becker	C-Core G-Grab		<b>V</b> -Vane	Legend Installation:	Bentoni	ite	Final Depth of Hole: 2	2.1
Legen Sample Type	е ЦДи-+ с					nistaliation.			Depth to Top of F	
Туре:	Sar	Lab Spoon	O-Odex (air rotary) W-Wash (mud retu	"")   []	T-Shelb	Cuttings	Piezom	neter		

		Ministry of						EST PIT LOG	Te	st Pit #: TP22-BR	A-0
BRI	TISH	Transportation	Project: B			nd F	Rest	Area		e(s) Drilled: March 2, 2022	
	ared by:	and Infrastructure 32079	Location: Ab Datum: UTM		BC			Alignment:	-	npany: On-Track Drilling Inc.	
Prepa	Thurber E	ingineering Ltd.	Northing/East		6628.	.36 .	5411	-		erator: Troy avator: Excavator	
Logge	d by: RM	Reviewed by:	Elevation:			,		Coordinates Surveyed			
_		XPocket Penetromete 100 200	Shear Strength	(kPa) ш	0	(%)	Ч		Z		
DEPTH (m)	DRILLING DETAILS	100 200	300 400	( <sup>kPa)</sup> EXPRIE TYPE	SAMPLE NO	RECOVERY (%)	SYMBOL	SOIL	CLASSIFICATION	COMMENTS	
H	TAI			Ш	ЪГ	ЧЩ.	SΥ	DESCRIPTION	EIC	TESTING	
Щ	DER	▲ SPT "N" (BL	OWS/300 mm) ▲ ⊻% Wi %	AMP	AM	8	SOIL	DESCRIPTION	ASS	Drillers Estimate	
		W <sub>P</sub> % ↓ V 20 ↓ 40	₩ 60 ₩L%	, do	S	RE	Š		5	{G % S % F %}	
0					1		///	OH - ORGANIC SILT, some sand, trace	ОН		
			78.2				1	rootlets, dark brown, soft.			
							H	0.61r	n	-	
								CL - SILTY CLAY, some sand, grey, stiff			
-1											
			····							Difficult digging with excavator	
				×	2				CL		
-2		22.4		· · · ·	2		///				
					4			2.29r	n		
								End of test pit at required depth. Test pit open to 2.3 m depth.	"		
								Seepage observed at 0.6 m depth during			
2								excavation.			
-3			••••••••••••••••••••••••••••••••••••••								
			<u></u>								
-4											
-5											
-											
			<u></u>								
-6											
-7			···· ÷··· ÷··								
			••••••••••••••••••••••••••••••••••••••								
			·····								
-8											
-			·····								
-9		·····	·····								
		·····									
10 Legen			<u></u>	···:···  la.c		1				Final Depth of Hole: 2	2 1
Legen Sampl	C	Auger 🔲 B-Becker 🗌		<b>G</b> -Grab	· · · ·	V-Va		Legend Installation: Grout Cement Bento		Depth to Top of F	
Type:	Sar	Lab Spoon Solit	O-Odex (air rotary)	<b>W</b> -Wash (mud retur	<u>_ ا</u>	T-Sh	nelby e	Drill Cuttings 🖽 Slotted 🔀 Slough 💽 Piezo	meter		

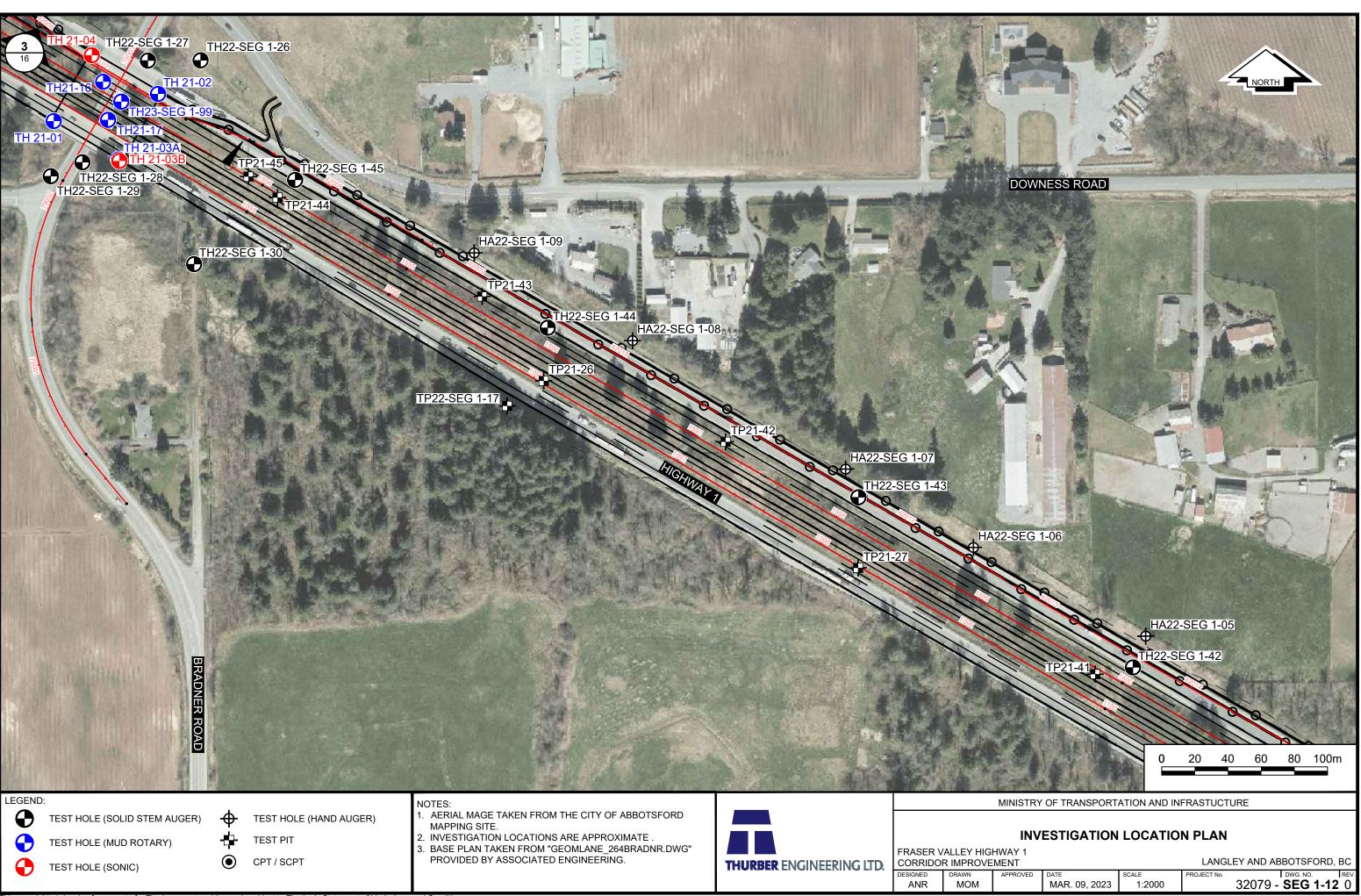
- MI		Ministry of						EST PIT LOG	Те	st Pit #: TP22-BR	A-0
BRI	TISH	Transportation	Project: E			ad F	Rest	Area		e(s) Drilled: March 2, 2022	
	UMBIA	and Infrastructure	Location: At					Alignment	-	npany: On-Track Drilling Inc.	
Prepa	ared by: Thurber E	32079 ngineering Ltd.	Northing/Eas			73	5/11	Alignment: 177.6 Station/Offset:		erator: Troy avator: Excavator	
l onne	d by: RM	Reviewed by:	Elevation:	ung. 04	00002		541	Coordinates Surveyed			
Loggo	u by: 1 th	XPocket Penetrometer 100 200		n (kPa) 🔒	<u>_</u> ا	<b>(</b> %			z		
Ξ	ဂိုလ်	100 200	300 400	%	SAMPLE NO	RECOVERY (%)	SYMBOL		CLASSIFICATION		
E	DRILLING DETAILS			Ľ	길끺	ĒR	NN	SOIL	FIC/	COMMENTS TESTING	
DEPTH (m)		▲ SPT "N" (BL	.OWS/300 mm) ▲	Ģ	ĮĮ	lo S		DESCRIPTION	SSII		
		<sup>₩</sup> ₽% 20 – 40	₩ • 60 • 80	6	ς δ	2 E C	SOIL		CLA	Drillers Estimate {G % S % F %}	
0					1	-	11	OH - ORGANIC SILT, some sand, trace	ОН		
			73.4		4		11	rootlets, dark brown, soft.			
							1				
			· • · · • • • • • • • • • • • • • • • •				H	0.76n	η <u> </u>	-	
1								CL - SILTY CLAY, some sand, grey, stiff to hard.			
			• • • • • • • • • • • • • •							Difficult digging with excavator	
				Π						Atterberg (Sa#2): PL:21% LL:31%	
		27.1			2			1	CL	I L.21/0 LL.J1/0	
2											
							¥	2.29n End of test pit at required depth.	ι <del> </del>	-	
								Test pit open to 0.8 m depth.			
								Seepage observed at 0.8 m depth during excavation.			
-3											
		····÷···÷··									
-4											
•											
-5											
		····									
-6											
				;							
,											
7		·····									
			· · · · · · · · · · · · · · · · · · ·								
8											
9											
<b>~</b>			· • · · • • • • • • • • • • • •								
10											
10 Legen	id [T5] • /	Auger <b>B</b> -Becker		G-Grab		<b>v</b> -v		Legend Installation: Sand Grout Cement Bento	I	Final Depth of Hole: 2	2.1
Sampl	C							in istaliation:		Depth to Top of F	
Type:	Sar	Lab Spoon	]0-Odex (air rotary)	W-Wash (mud ret	ırn) 🖽	T-SI	ныру Ю	Drill Cuttings 🖽 Slotted 🔀 Slough 🐼 Piezo	meter		



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This copyrighted drawing forms part of a Thurber report and its use is subject to Thurber's Statement of Limitations and Conditions

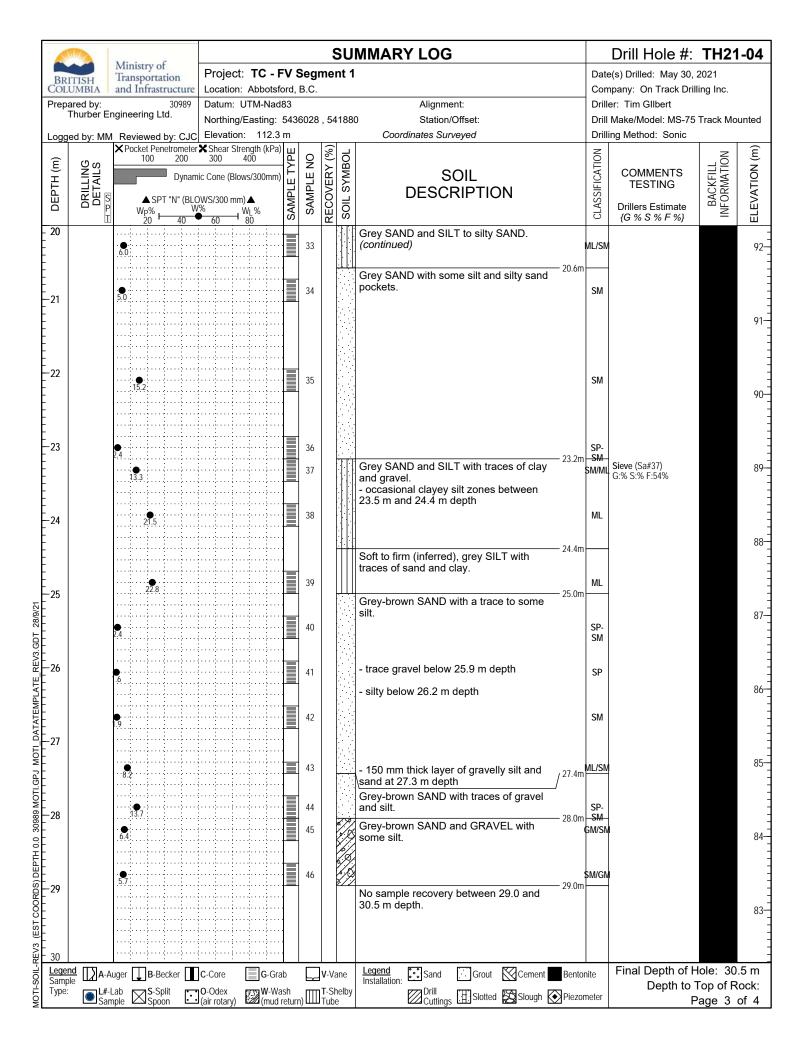


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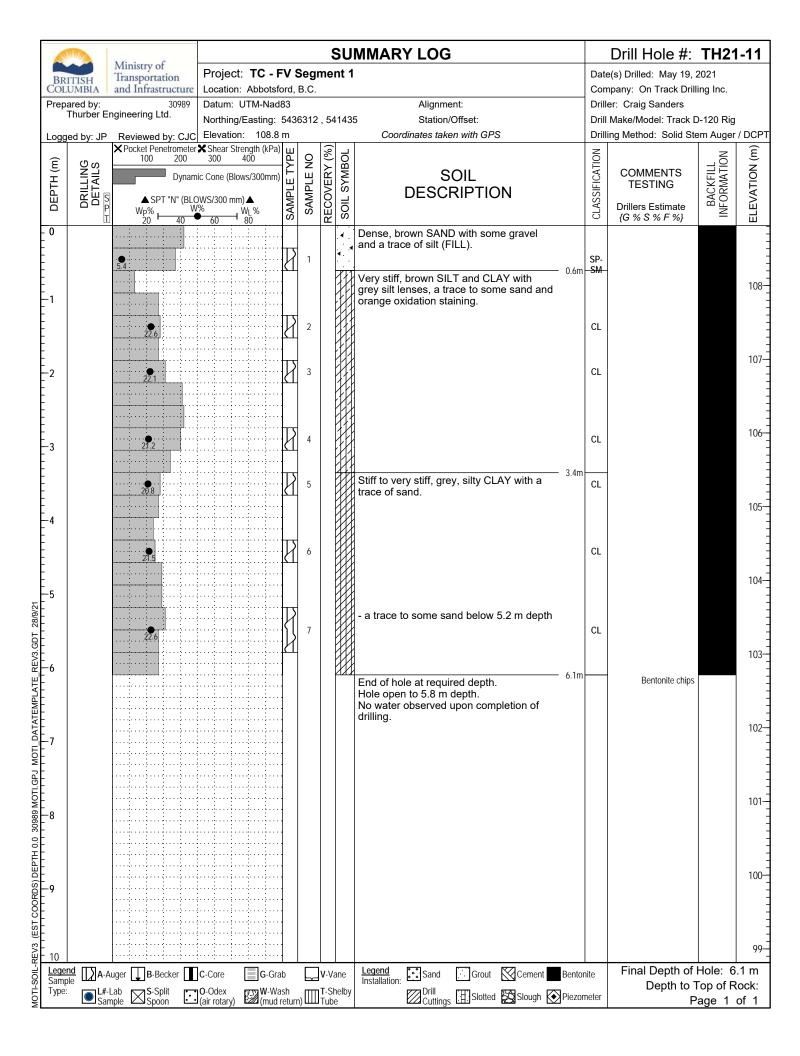
MENI			LANGLEY AND AB	BUISFURD,	BC
APPROVED	DATE MAR. 09, 2023	scale 1:2000	PROJECT No. 32079 -	DWG. NO. SEG 1-12	REV.

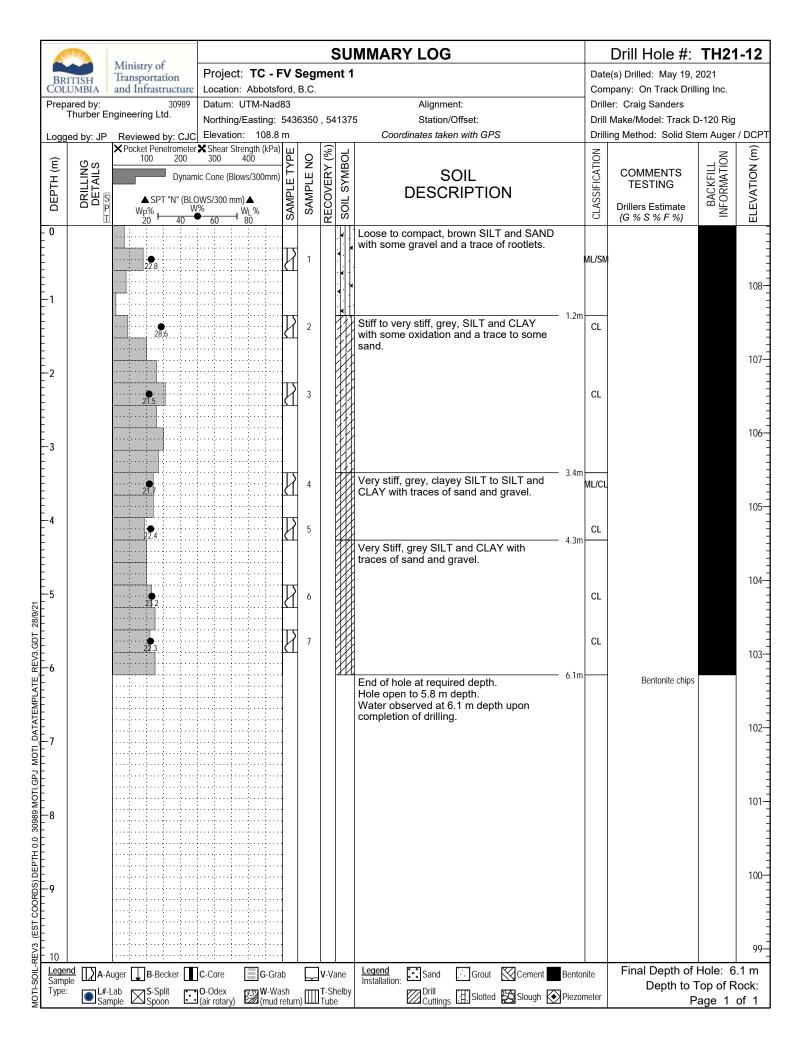
		NO C				S	U	MMARY LOG			Drill Hole #:	TH21	-0
BRI	TISH	Ministry of Transportation	Project: TC - F	=V :	Seg	men	t 1				e(s) Drilled: May 30, 2		
COLL	JMBIA	and Infrastructure	Location: Abbotsf		B.C.					-	npany: On Track Drill	ing Inc.	
	ared by: Thurber Fr	30989 ngineering Ltd.	Datum: UTM-Nad					Alignment:			er: Tim Gllbert		
		0 0	Northing/Easting:	543	6028	3 , 541	880				Make/Model: MS-75	Track Mo	unte
Logge	ed by: MM	Reviewed by: CJC	Elevation: 112.3	m 1				Coordinates Surveyed			ing Method: Sonic		
Ê	ის	Reviewed by: CJC Pocket Penetrometer 100 200 Dvnam	300 400	Į Ę	9	RECOVERY (%)	SYMBOL			CLASSIFICATION		BACKFILL INFORMATION	<u>؟</u>
DEPTH (m)	DRILLING DETAILS	Dynam	ic Cone (Blows/300mm)	lн	SAMPLE NO		ž	SOIL		ICA_	COMMENTS TESTING	AT AT	
FT	N ET	▲ SPT "N" (BLC	W/S/200 mm) ▲	ЪП	MPI	No.		DESCRIPTION		SSIF	TESTING	ACK	
B			% _ WL%	SAMPLE	SAI	Ш	SOIL			CLAS	Drillers Estimate	NF(	l 1
0	Τ	20 40	60 80	0,		2		ASPHALT (254 mm thick).		$\vdash$	{G % S % F %}		
Ŭ					1		. Ų .		0.3m,	sw/gv			1
		9.8			2	ľ	0	Grey-brown SAND and GRAVEL with trace to some silt, a trace of cobbles and		GM/SN			
		15.5			- <sup>2</sup>		Pri	· · · · · · · · · · · · · · · · · · ·	0.7m		Atterberg (Sa#3):		
1		·····			3	IE		Firm to stiff (inferred), brown SILT and		CL	PL:19% LL:36%		
					-			CLAY with traces of gravel and sand (FILL).					
		21.0			4			()-	1.5	CL	Sieve (Sa#4) G:% S:% F:73%		1
						0.	<u>.</u>	Grey-brown GRAVEL and SAND to	1.5m				
		•		1	5	e	ې :	gravelly SAND with a trace to some silt (FILL)		GM/SN			
2		5.7			<b>,</b>	. ·	0	(FILL)					
		16.6			6		o O	- a trace to some clay between 2.1 m and		gm/sn	Sieve (Sa#7)		-
		8.0			7			2.2 m depth		\$M/GN	G:% S:% F:9%		
		0.0			8		, N			SP/GP			
		4.6				Ь.	。						
3						o.	0						
		••••••••		1	9	e	γQ			SP-			1
		3.2		•	Ĺ		0			GP			
							0						
-4					-		0						
						ė.	0. ^						
					10	p.	ي ہ ہ			SM			1
		8.8				0.	0						l
				1	-	6	<u>. 6</u>		4.9m		ļ		l
5					11	0.	0	Grey-brown, sandy GRAVEL to GRAVEL and SAND with a trace to some silt		GP-			l
		4.9			4		0	(FILL).		GM			1
		•			12	0.	0. ^			GM			
		7.7			. <u>~</u>	Ιb.	) 0						
6						, i , i	0						
-		4.9		•	13	i	0			GP/SP	1		
					14		0			GM			
		2.7			15	0. . e	اير			\$M/GN	4		l
		<b>9</b>			16	Þ.	0			SP/GP			l
7					17			Grey-brown, sandy SILT to SAND and	7.0m	SC/CL	1		
		24.0			1			SILT with a trace to some clay and a			Sieve (Sa#A)		1
		31.9			A			trace of organics.			G:% S:% F:59% Atterberg (Sa#B):		l
					1			Grey-brown SILT with traces of sand, clay	7.6m		PL:24% LL:29%		
8				•	В		$\ \ \ $	and organics.		ML	Sieve (Sa#B) G:% S:% F:91%		
-							$\ \ \ $				Atterberg (Sa#18):		
							$\ \ \ $				PL:26% LL:31%		
		<b></b>			18		$\ \ \ $			ML			
		27.8					$\ \ \ $						
9		···· : ···· : ··· : ··· : ··· : ··· : ··· : ··· : ··· : ··· : ··· : ··· : ··· : ·	·····.						0.1~				
					19			Firm (inferred), grey SILT with traces of	9.1m	OL/ML			1
				-	1		$\ \ \ $	clay and sand and zones of organic silt.	o <i>í</i>		Atterberg (Sa#20):		
			•••••		20				9.6m	CL	PL:17% LL:27%		
10		24.0	<u></u>										
Legen Sampl	A-A		C-Core G-Gra	ab		V-Var	ne	Legend Installation: Sand Grout Cement	Bento	nite	Final Depth of H		
Sampi Type:	🗖 L#-l	_ab 🔽 S-Split 📑	O-Odex (air rotary)	ash	, IIII	T-She	elby	Drill Slotted Slough	Piezor	neter	Depth to T		
	San	אט Spoon שי Spoon	(air rotary) 🚧 (mud	retur	n) Ш	lube			. 10201		P	age 1 (	of

	MILLES .					SU	MMARY LOG		Drill Hole #:	TH21	1-04
BRI	TISH	Ministry of Transportation	Project: TC -	FV	Seg	ment '	1	Dat	e(s) Drilled: May 30, 2	2021	
COLL	JMBIA	and Infrastructure	Location: Abbots		B.C.			_	mpany: On Track Drill	ing Inc.	
Prepa ۲	ared by: Thurber Er	30989 ngineering Ltd.	Datum: UTM-Nac	183	6000	EAAO	Alignment:		ler: Tim Gllbert	Track	
		Reviewed by: CJC Pocket Penetrometer 100 200 Dynam	Northing/Easting:	543 3 m	oU28	, 54188	30 Station/Offset: Coordinates Surveyed		I Make/Model: MS-75 ling Method: Sonic	I rack Mo	ounte
LUgge	eu by. Iviivi	×Pocket Penetrometer	Shear Strength (kPa	) ш		<u>_</u>		-		~	Ê
DEPTH (m)	L S D	100 200	300 400	۲F	SAMPLE NO	RECOVERY (%) SOIL SYMBOL	2011	CLASSIFICATION	COMMENTS	BACKFILL INFORMATION	
H	DRILLING DETAILS	Dynam	nic Cone (Blows/300mm	Ш	PLE	SYN SYN	SOIL DESCRIPTION	IFIC	TESTING	CKF RMA	EI EVATION (m)
Ш	R B B	▲ SPT "N" (BLC W <sub>P</sub> % W	OWS/300 mm) ▲ /% WL %	SAMPLE	SAM	SOIL	DESCRIPTION	ASS	Drillers Estimate	BA	
10	Т	20 40	60 80					U	{G % S % F %}	<u> </u>	ū
		•			21		Soft (inferred), grey, clayey SILT to SILT and CLAY with some sand and a trace of	ML/CI			1(
		23.6					organics. <i>(continued)</i>				
			······································				Firm to stiff (inferred), grey SILT and	n	-		
11							CLAY with a trace to some sand and a trace of gravel.		Atterberg (Sa#22): PL:18% LL:36%		
		23.7		:1	22			CL	1 2.10/0 22.00/0		1
		····	·····								
12											
											1
					23						
		22.2			23			CL			
13				• •							
					24			CL			
					1						
14											
		17.3			25		- very stiff (inferred) below 14.5 m depth	CL			
15											
		·····									
					24						
		14.6			26		Grey GRAVEL and SAND, silty to some		-		
16		7.7		:	27		silt.	GM/SI	M		
							16.5				
		<b>9</b>			28		Grey SAND with a trace to some silt and	SP-			
17					1		gravel.	SM			
17		•••••••••••••••••••••••••••••••••••••••			29			SP			
		7			27						
		·····		• •							
18				: <u> </u>							
10		10.5		•	30			SP			
					1						
			· · · · · · · · · · · · · · · · · · ·		31			SP-			
19		10.6					- some silt to silty below 18.9 m depth	SM			
"					-						
		11.3			32			SM			
20			······································				Grey SAND and SILT to silty SAND.	n			
<mark>Legen</mark> Sampl	id A-A	uger 🔲 B-Becker	C-Core G-Gr	ab		V-Vane	Legend Installation: Sand Grout Cement Ben	onite	Final Depth of H		
Type:	L#-L Sam	ab Spoon	O-Odex (air rotary)	ash	ш	T-Shelby	Drill Cuttings Slotted Slough Piez	motor	Depth to T	op of R age 2	COC

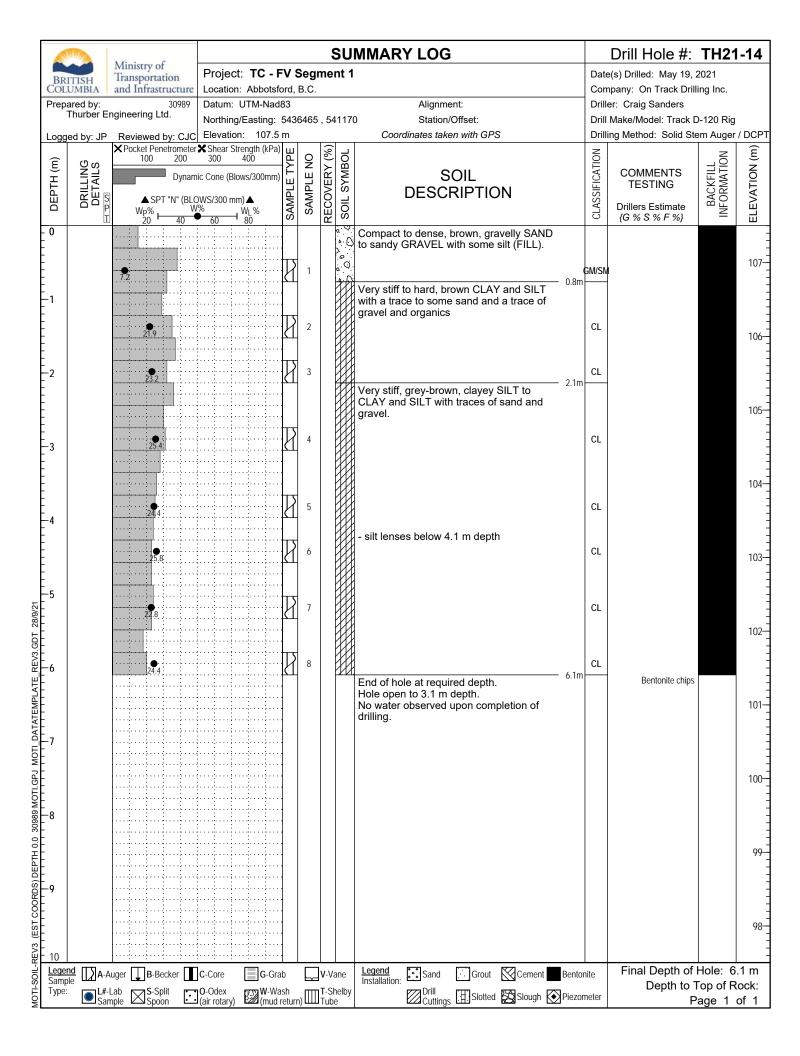


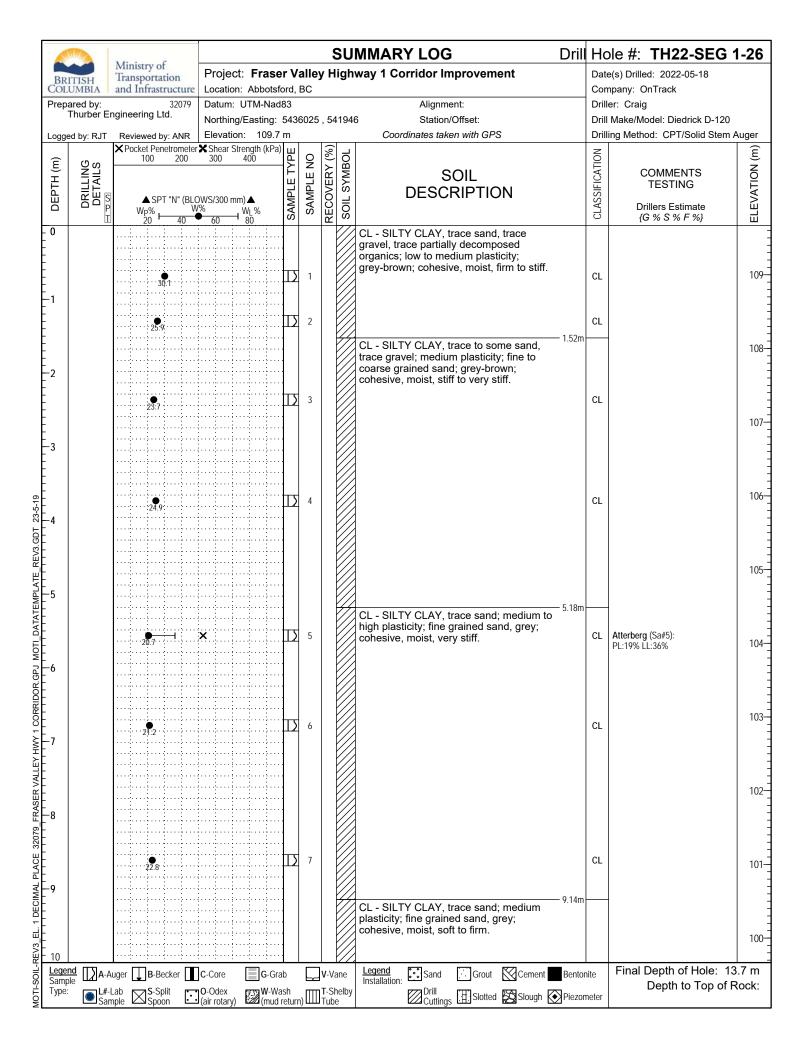
	MID .					Ś	SU	MMARY LOG			Drill Hole #:	<b>TH21</b>	-04
RPI	TISH	Ministry of Transportation	Project: TC - F	=V :	Seg					Date	e(s) Drilled: May 30, 2	2021	
	JMBIA	and Infrastructure	Location: Abbotsf	ord,	B.C.					Con	npany: On Track Drill	ing Inc.	
Prepa ר	ared by: Thurber Fr	30989 ngineering Ltd.	Datum: UTM-Nad					Alignment:			er: Tim Gllbert		
			Northing/Easting:		6028	3,54	11880				Make/Model: MS-75	Track Mo	unted
Logge	ed by: MM	Reviewed by: CJC	Elevation: 112.3	m	1			Coordinates Surveyed			ing Method: Sonic		
Ê	() ()	Pocket Penetrometer 100 200 Dynam ▲ SPT "N" (BLC W <sub>P</sub> % W 20 40	300 400	١Ę	9	RECOVERY (%)	SYMBOL			CLASSIFICATION		BACKFILL INFORMATION	ELEVATION (m)
5 T	AILS	Dynam	ic Cone (Blows/300mm)	Ē	Щ	RY	ž	SOIL		CAT	COMMENTS	EILI IATI	
DEPTH (m)				Ы	JPL	N	S.	DESCRIPTION		SIFI	TESTING	ACK	AT
	DRILLING DETAILS	▲ SPT "N" (BLC WD% W	20WS/300 mm) ▲ 20 Wi %	AM	SAMPLE NO	1 N	SOIL			LAS	Drillers Estimate	B/ NFC	ļй
30	T	W <sub>P</sub> % W 20 40	₩L% 60 80	S		R	ω σ			0	{G % S % F %}	_	Ξ
30				•				No sample recovery between 29.0 and 30.5 m depth. <i>(continued)</i>					8
				1					— 30.5m		Dontonito obino		0
				-				End of hole at required depth.			Bentonite chips		
				1									
31				-									
				1									8
		····‡···‡···‡···‡···		-									
				1									
32				-									
				1									8
				]									
				1									
				1									
33				-									
				1									7
				-									
				1									
34				]									
				-									_
		·····		1									7
				-									
				1									
35				-									
				1									7
				]									
				1									
36				1									
50				1									
		· · · · · · · · · · · · · · · · · · ·		1									7
				-									
				1									
37													
				1									7
				]									
				1									
				1									
38		····		1									
				1									7
				-									
				1									
39				1									
				-									-
				1									7
				-									
10		····		1									
40 _egen	d TTA A			1		<b>V</b> -Va	1	Legend Installation: Sand Grout Cement	Ponter	nite	Final Depth of H	ole: 30	.5 m
Legen Sampl		uger 🔲 B-Becker 🔳									Depth to T		
Туре:	Sam	_ab ⊠ <mark>S</mark> -Split ⊡	O-Odex (air rotary)	1511 retur	n) Ш		e	Drill Cuttings	Piezon	neter		age 4	



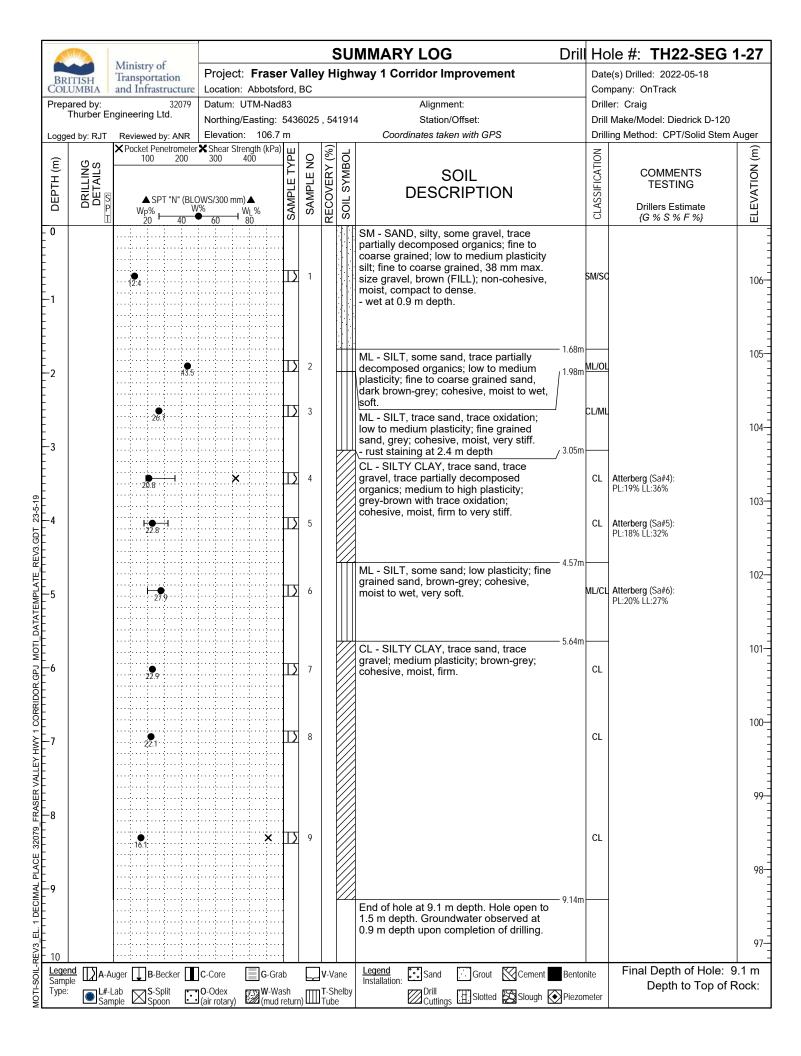


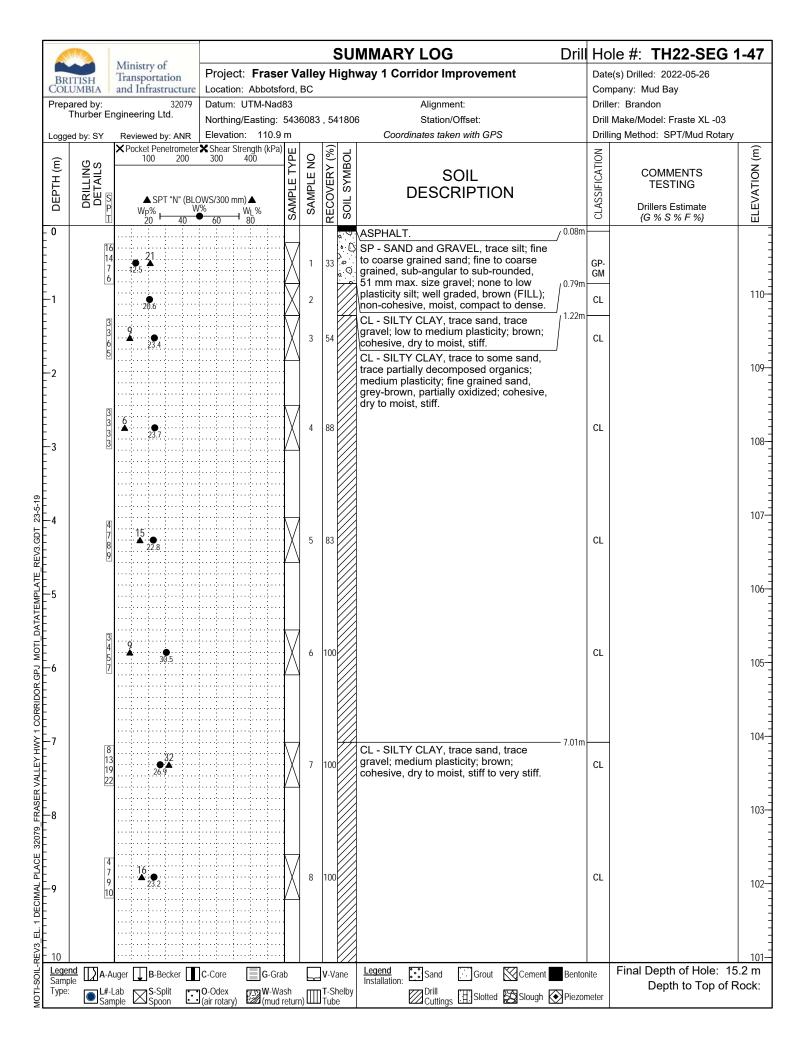
		NC				5	<u>SU</u>	MMARY LOG		Drill Hole #: Th	<u> 121-1</u>		
BRI	TISH	Ministry of Transportation								Date(s) Drilled: May 19, 2021			
COLUMBIA and Infrastructure			Location: Abbotsford, B.C.					_	Company: On Track Drilling Inc.				
Prepared by: 30989 Thurber Engineering Ltd. Northing/Easting: 543					o 4 o o	- 4	400	Alignment:		riller: Craig Sanders	D D		
			Elevation: 107.7	543 m	0400	, 54	120	3 Station/Offset: Coordinates taken with GPS		vrill Make/Model: Track D-120 vrilling Method:  Solid Stem A	•		
LUgge	su by. Jr	×Pocket Penetrometer	Shear Strength (kPa)	ш	_	(%	Ļ		-		-		
E	2 V V V	Reviewed by: CJC Pocket Penetrometer 100 200 Dynam	300 400	ТҮР	SAMPLE NO	RECOVERY (%)	SYMBOL	601	CI ASSIEICATION				
DEPTH	DRILLING DETAILS	Dynam	DWS/300 mm)▲		РГЕ	VER	SYN	SOIL DESCRIPTION			SMA T		
ШЦ		▲ SPT "N" (BLC			AM	Ő	SOIL	DESCRIPTION		A A A Drillers Estimate	FOF		
	Ť		<sup>1%</sup> ₩L%	S₽	S	RE	Š		C	G % S % F %}	≤ ī		
0							•	Dark brown ORGANIC SILT with some gravel and a trace to some clay and sand.					
			•	$\mathbf{V}$	1				0	н			
			54.8	Г							1		
1							•  *						
'		····						1.2r	nL				
		26.5		R	2			Very stiff to hard, Grey-brown, clayey	CL				
								sand and mixed zones of sandy silt	M		1		
_													
2				$\mathbb{H}$				2.1r Very stiff to hard, grey-brown SILT and		_			
		24.4		И	3			CLAY with traces of sand, organics and	C				
								oxidation staining.					
		22.2		$\mathbf{V}$	4			- a trace of gravel below 2.8 m depth	c	L			
3				Г				5					
								3.7	nL				
		21.1		K	5			Very stiff to hard, grey-brown, SILT and CLAY with trace to some sand and mixed	"ML/	СГ			
4				1	6			zones of silty sand.	c	L			
		21.4		Щ									
5													
		•		$\nabla$	7			Very stiff, grey SILT and CLAY with 5.2r	n c	L			
		24.2		Н				traces of sand and gravel					
6								6.1	nL				
								End of hole at required depth.		Bentonite chips			
				1				Water observed at 4.0 m depth upon					
								completion of drilling.					
7													
		···· ···· ··· ··· ··· ··· ··· ··· ···	······································										
				1									
8													
9													
		·····	······										
			· · · · · · · · · · · · · · · · · · ·										
10													
Legen Sampl	A-A	uger 🚺 B-Becker 🚺	C-Core	b	F	V-Va	ane	Legend Installation: Sand Grout Cement Bent	onite	Final Depth of Hole			
Sampi Type:	C		O-Odex (air rotary)	sh				Drill Cuttings Slotted Slough Piezo		Depth to Top			
	San	npie 🖂 Spoon 🕒	air rotary)	returr	η) ШШ	lube	9			~   Page	e 1 of		

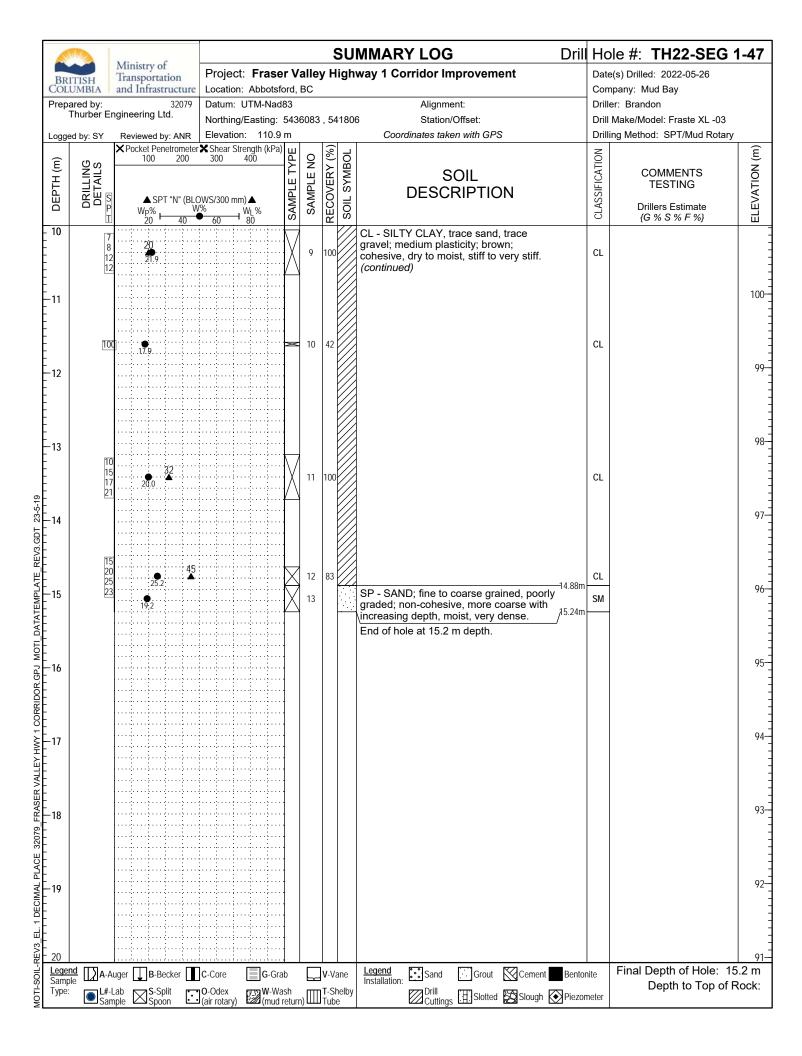




-	1100	Ministry of			SL	JMMARY LOG Dr	II Ho	ole #: TH22-SEG	1-2		
BRITISH Transportation		Transportation	Project: Fraser Valley Highway 1 Corridor Improvement					Date(s) Drilled: 2022-05-18			
COLUMBIA and Infrastructure			Location: Abbotsford, BC Datum: UTM-Nad83 Alignment:					mpany: OnTrack			
Prepared by: 32079 Thurber Engineering Ltd. Datum: UTM-Nad83 Northing/Easting: 5436025, 5419					E E410			ler: Craig			
			Elevation: 100.7 m		5, 54194	46 Station/Offset: Coordinates taken with GPS		I Make/Model: Diedrick D-120 ling Method: CPT/Solid Stem			
Logge	d by: RJT	Reviewed by: ANR Pocket Penetrometer	Shear Strength (kPa)	1	()		-				
Ê	იღ	100 200	X Shear Strength (kPa)           300         400           WS/300 mm)           WS/300 mm)           WK %           60	SAMPLE NO	RECOVERY (%) SOIL SYMBOL		CLASSIFICATION				
Ĕ	DRILLING DETAILS			<u>і</u> Ш	ΓR Σ	SOIL	ICA	COMMENTS TESTING			
DEPTH (m)	<u>a</u> E E	▲ SPT "N" (BLC	)WS/300 mm) ▲	:  ₹		DESCRIPTION	SSIF	TESTING			
۵I	DR DE	W <sub>P</sub> % W	0WS/300 mm) ▲ % WL% 60 80	SA	SOIL		CLAS	Drillers Estimate { <i>G</i> % <i>S</i> % <i>F</i> %}			
10	L					CL - SILTY CLAY, trace sand; medium	CL				
		22.8	····	4 °		plasticity; fine grained sand, grey;		PL:17% LL:29%			
						cohesive, moist, soft to firm. (continued)					
.11											
		····				CL - SILTY CLAY, trace sand, trace	n	-			
						aravel: medium to high plasticity: grey:					
				5 9		cohesive, moist, firm.					
		22.5	··················	4 '			CL				
12											
						- density of clay becomes very stiff to					
						hard at 12.2 m depth					
		19;2		<u>Σ</u> 10			CL				
13		19,2									
		·····									
		····				End of hole at 13.7 m depth. Hole open to	n	_			
14						13.6 m depth. Ground water observed at					
						4.9 m depth upon completion of drilling.					
15											
		····									
16											
10											
17											
		·····									
10											
18											
19											
20											
	<u>id</u> ∏∑l∆.∧	Auger 🔲 B-Becker 🚺	C-Core G-Grab		V-Vane	Legend Installation Sand Grout Cement Ben	onite	Final Depth of Hole: 13	3.7		
<u>Legen</u> Sampl Type:								Depth to Top of F			
JPC.	Sar	Lab S-Split 🖸	O-Odex W-Wash (air rotary) (mud retu	(Inn)		y Drill Slotted Slough Neiz	ometer	1			



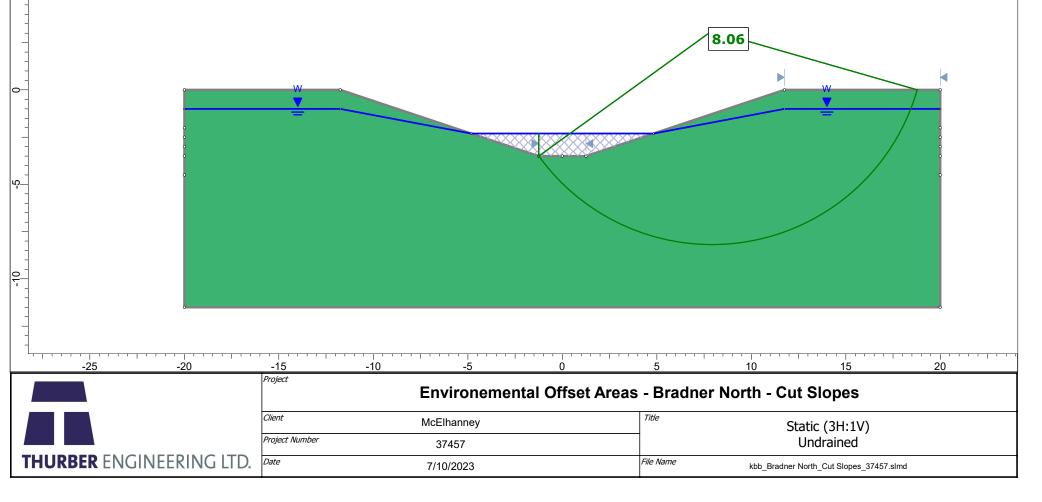


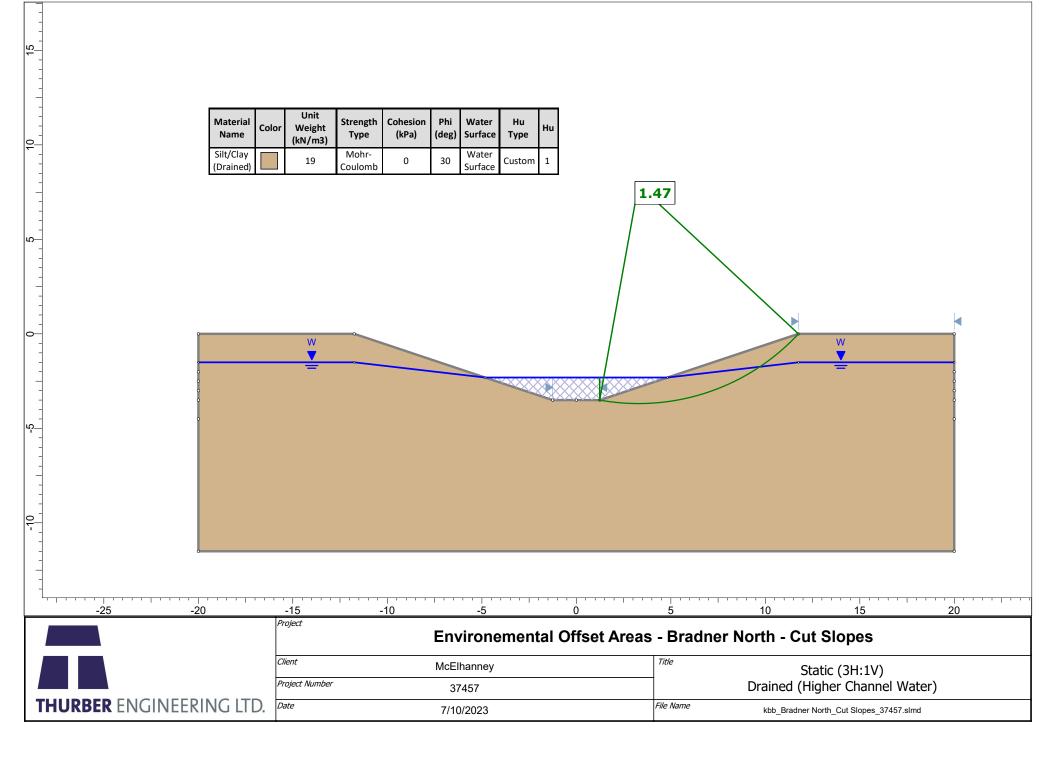


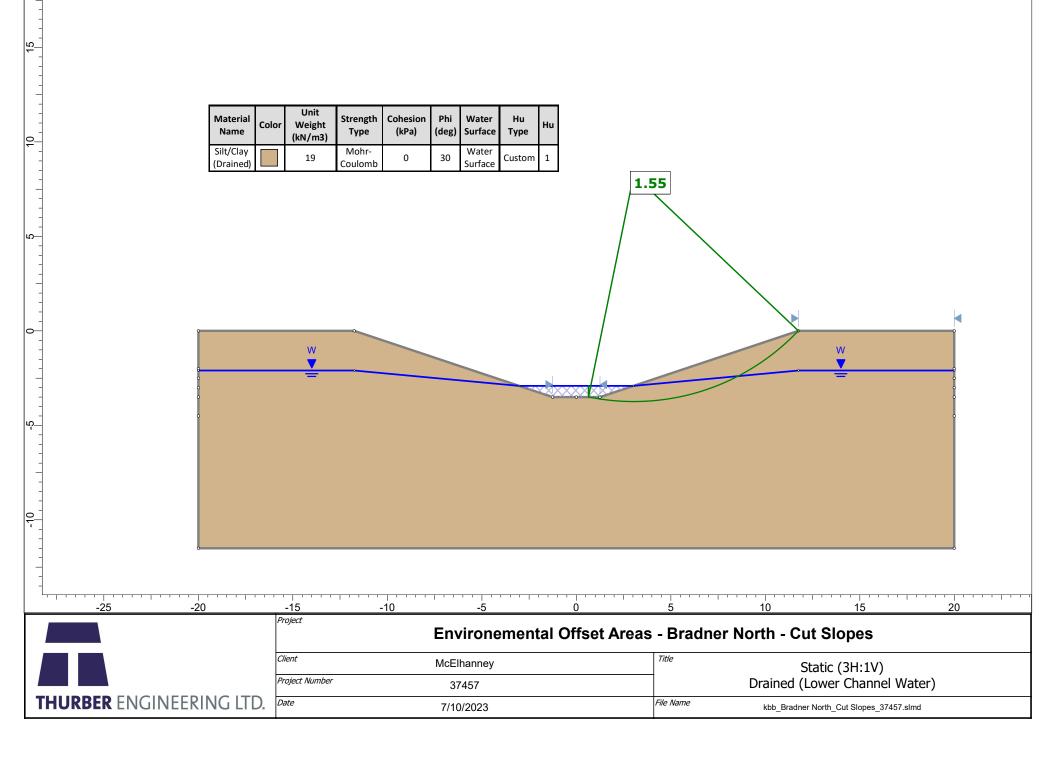
Materia Name	Color	Unit Weight (kN/m3)	Strength Type	Cohesion (kPa)	Cohesion Type	Water Surface	Hu Type	Hu
Silt/Clay		19	Undrained	75	Constant	Water Surface	Custom	1

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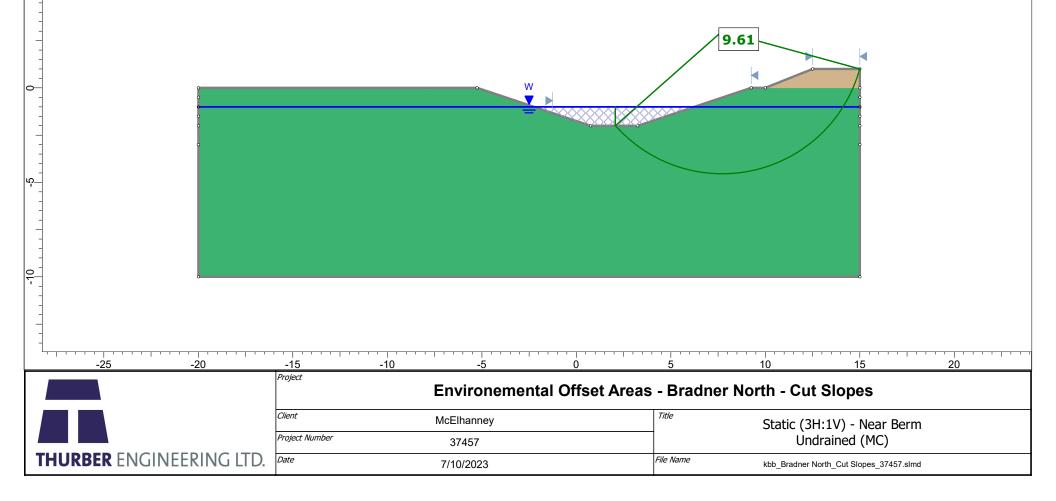


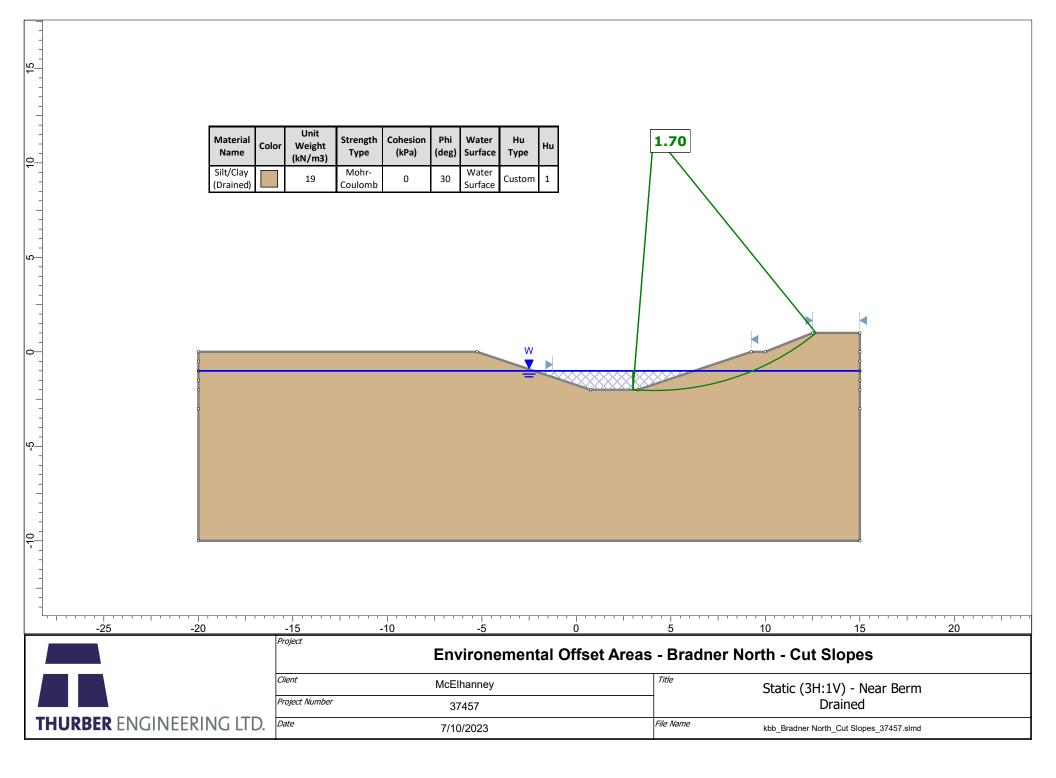


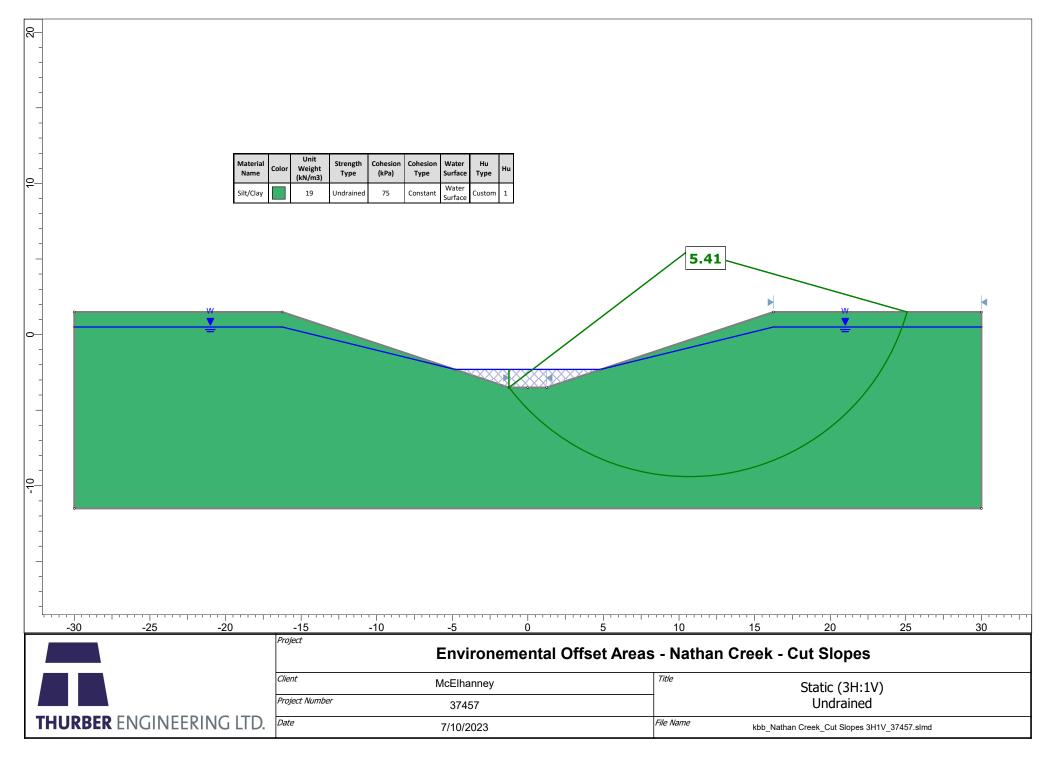
Material Name	Color	Unit Weight (kN/m3)	Strength Type	Cohesion (kPa)	Phi (deg)	Cohesion Type	Water Surface	Hu Type	Hu
Silt/Clay		19	Undrained	75		Constant	Water Surface	Custom	1
Silt/Clay (Drained)		19	Mohr- Coulomb	0	30		Water Surface	Custom	1

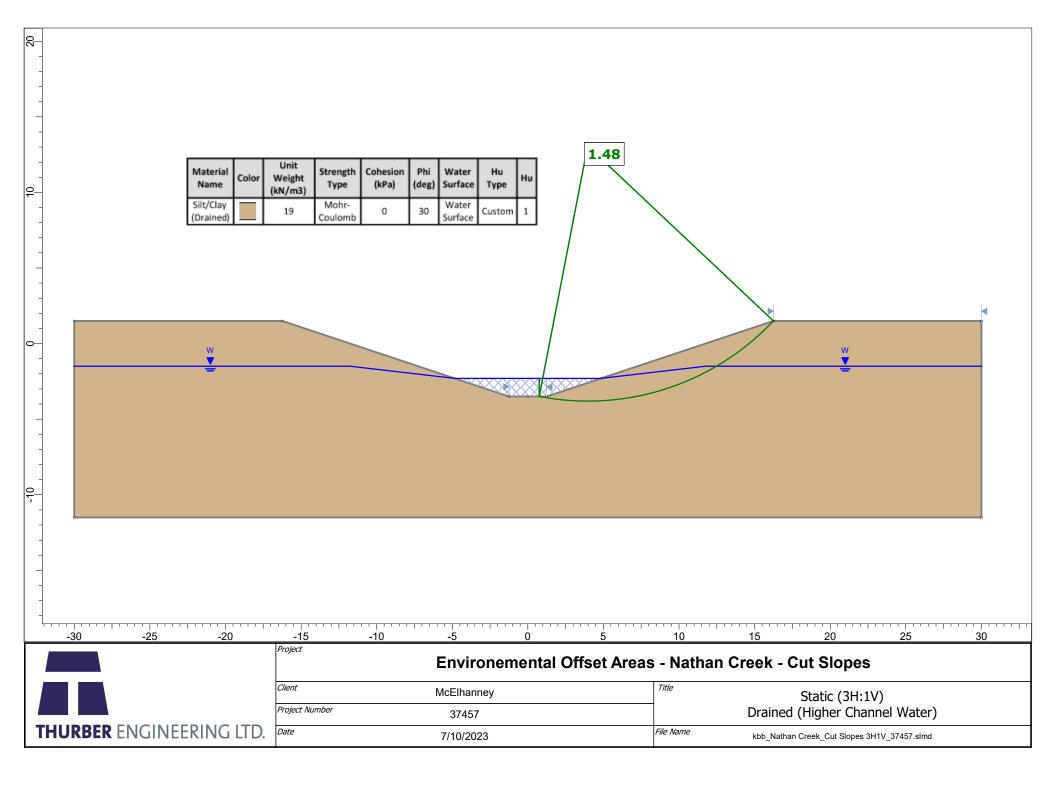
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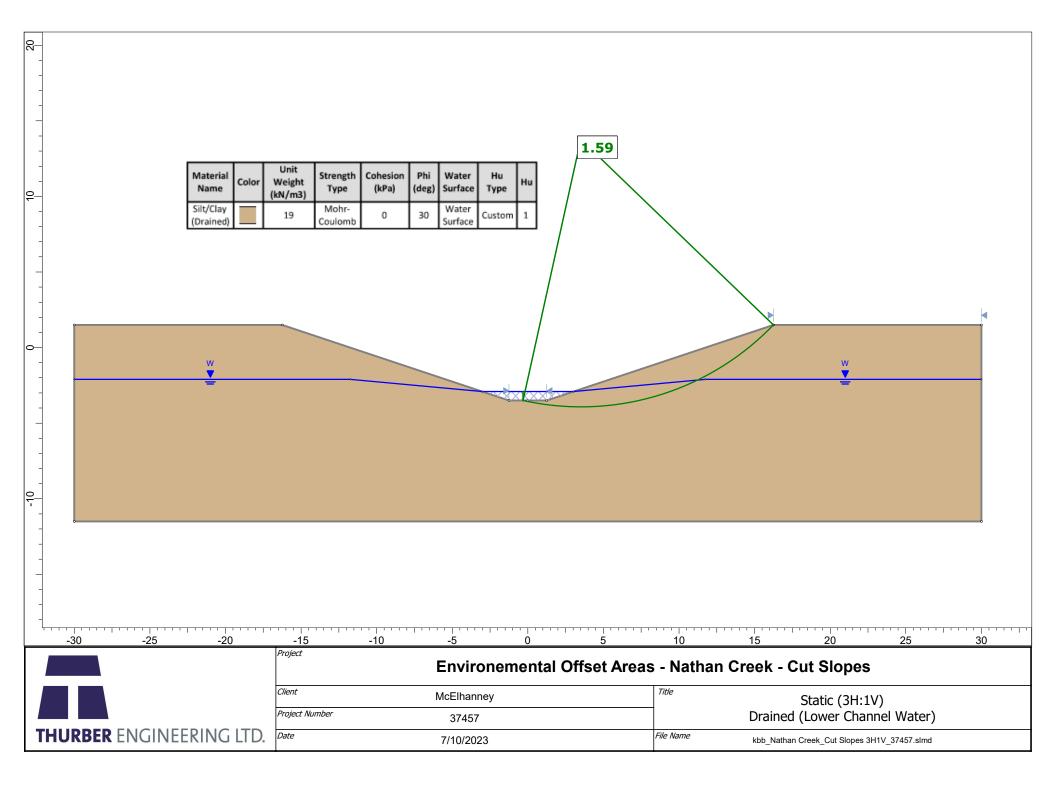
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Material Name	Color		Strength Type	Cohesion (kPa)	Phi (deg)	Cohesion Type	Water Surface	Hu Type	Hu
Silt/Clay		19	Undrained	75		Constant	Water Surface	Custom	1
Rip Rap		22	Mohr- Coulomb	0	45		Water Surface	Custom	1

